

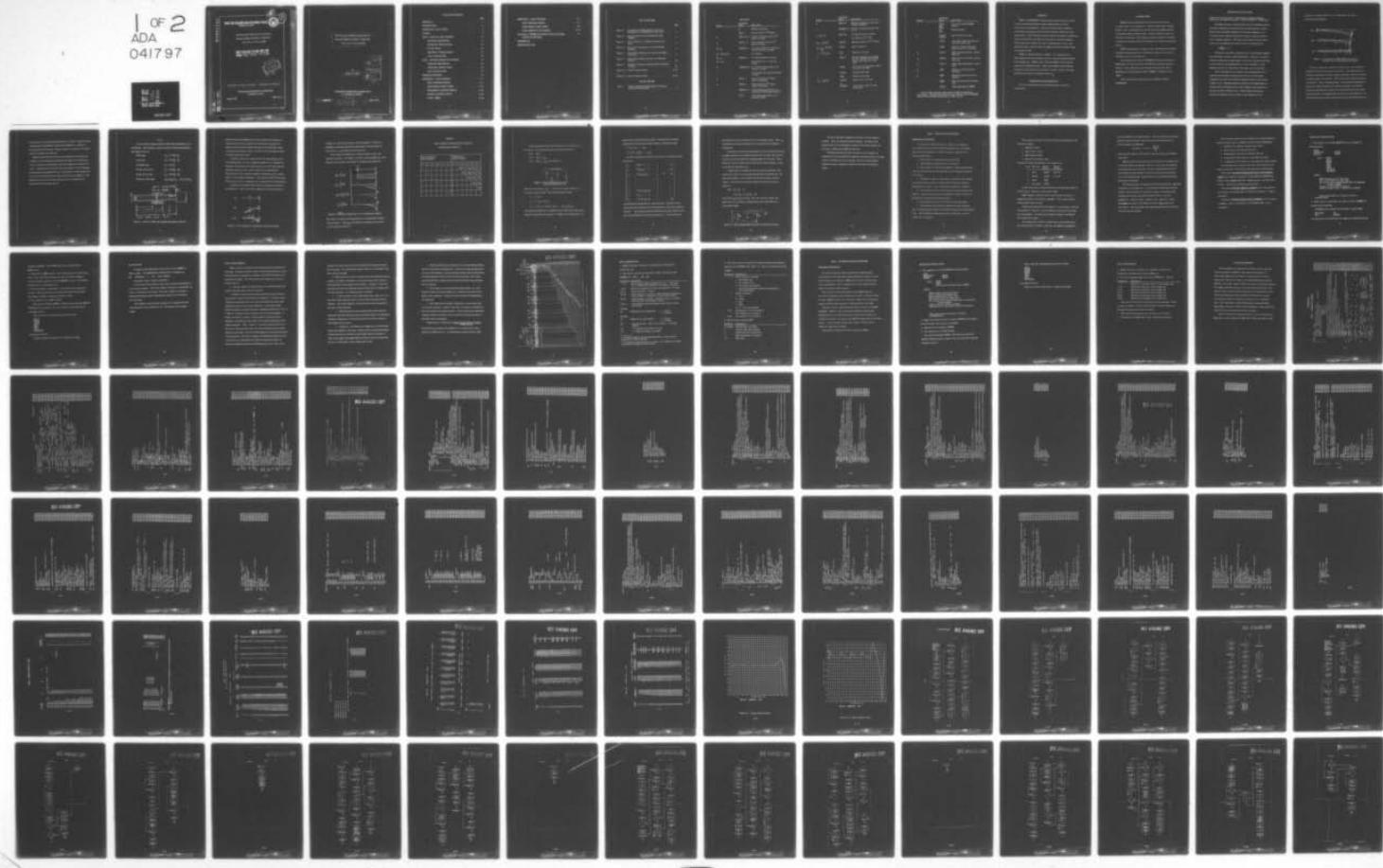
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SHIP PROPULSION SHAFTING BEARING REACTION PROGRAMS MGE2 AND MGE--ETC(U)  
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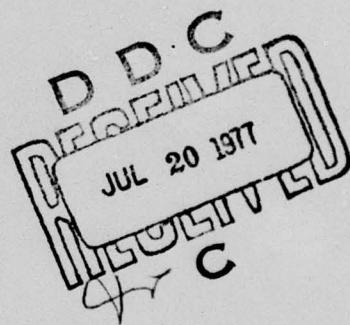


Ship Propulsion Shafting Bearing Reaction

Programs MGE2 and MGE5 for IBM 7090

(with notes on Univac LARC)

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## APPLIED MATHEMATICS LABORATORY TECHNICAL NOTE

August 1967

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⑩ Sharon E. Good

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## NOTATION

<u>Symbol</u>	<u>FORTRAN Name</u>	<u>Description</u>
	N	Number of stations.
	NO (I)	Station number of I <sup>th</sup> station.
x <sub>i</sub>	DISTL (I), A	Length to extreme end from I <sup>th</sup> station in inches.
d <sub>a</sub>	DIA (I), B	Outer diameter of shaft at I <sup>th</sup> station in inches.
(a) d <sub>b</sub>	STIFX(I), C	(a) Inner (if hollow) or second (if sleeve) diameter in inches.
(b) $\Sigma EI$ or ST		(b) Stiffness.
(a) d <sub>c</sub>	WTS(I), D	(a) Third diameter in inches.
(b) $\Sigma A_s$		(b) Weight in lb./in. per unit length.
W	CONWT(I), E	(a) Concentrated Weights in lbs. (negative in sign).  (b) and Bearing reactions (positive in sign).
a	IM (I), I	Outer material at I <sup>th</sup> station (only 1-5 possible).
b	JM (I), J	Inner material at I <sup>th</sup> station (only 1-5 possible).
	IBRG(I), K	Code indicating presence (1) or absence (0) of bearing at station I.
	IS (I)	Code indicating sand (1) or no sand (0) in bore.

Symbol	FORTRAN Name	Description
E	YMAT, H	Moduli of elasticity in lbs./sq. in. (Young's modulus).
$\rho$	DENMAT, P	Density of shaft materials in lbs./cu. in.
$l_i = x_{i+1} - x_i$	DIST T(I)	(a) Section length in inches. (b) Stiffness ( $10^{-10}/EI$ )
$M_L = \int_0^L S dL$	BMTAB	Bending moment in $10^{-3}$ inch-lbs.
$\theta_L = \frac{1}{EI} \int_0^L M dL$	THE TA	Slope in Radians.
$\delta_L = \int_0^L \theta_L dL$	DEF	Deflection in inches.
$\alpha$	BNFLU	Influence numbers for bearings (lb. per .001-inch rise) and deflection and slope (for 1-inch rise).
	DIBRG	Section length from support point to extreme end table.
	IBTAB	Bearing index table.
n	IBRS	Number of bearings.
$S_L = \int_0^L W dL$	SFTAB	Shear force in $10^{-3}$ lbs.
	I2	
	IERROR	Error code in incorrect data preparation.

<u>Symbol</u>	<u>FORTRAN</u> Name	<u>Description</u>
	TITL2 IXM SWAT NS IYM	Case title array for MGE2. Sentinel Unused options.
R	CANOT CONOT	Bearing Reaction in lbs.
	WBAR	Total Shaft weight including concentrated loads in lbs.
	XBAR	Distance of Center-of-gravity from station no. 1 in inches.
$A_a$	AREA 1	Shaft cross section area, second material.
$A_b$	AREA 2	Shaft cross section area, second material.
$A_c$	AREA 3	Shaft cross section area, sand in bore.
$I_a$	AMI1	Moment of Inertia for first material.
$I_b$	AMI2	Moment of Inertia for second material.
	XBRG	Bearing relocation off straight line.
	TITL5	Case title array for MGE5.

Some storage areas have uses a and b in different sections of the program. The several arrays which have special names in READIN subroutine are listed as second entry in name column.

## ABSTRACT

MGE2 is a FORTRAN IV program which computes characteristics of the main propulsion shaft of a ship, assuming that all bearing centers are on a straight line. Output from this program consists of the straight-line bearing reactions and the influence numbers for each support point. These influence numbers indicate the changes in supporting reactions produced by the raising or lowering of a particular bearing. The program also calculates the shear, bending moment, slope, and deflection values, and the weight and stiffness factors for stations designated along the shaft.

MGE5 is a program similar to MGE2. It is a design tool for determining the effects of bearing centers at any given elevation relative to the straight line. MGE5 is often used after MGE2 to determine the reactions of realigned bearings. Output from MGE5 includes bearing reactions at each support point and shear, bending moment, and slope and deflections values at designated stations.

## ADMINISTRATIVE INFORMATION

The work reported herein was authorized under job number  
1-890-202-01.

## INTRODUCTION

**MGE2** gives the characteristics of a shaft with all bearings, or support points, on a straight line. Output includes shear, bending moment, slope, and deflection as well as weight and stiffness factors at designated stations along the shaft. A table of influence numbers is listed for each bearing. These influence numbers indicate the changes in supporting reactions caused by the raising or lowering of a particular bearing.

**MGE5** calculates shear, moment, slope, and deflection at various stations and bearing reactions, with bearing centers set in any given elevation relative to a straight line.

The programs were coded in **FORTRAN IV** with the exception of **MAP** double precision routines in the 7090 matrix inversion portion. Decks or further information are available from Code 830, Naval Ship Research and Development Center (NSRDC), Washington, D. C. 20007.

These programs have also been run on LARC and 7090 in **FORTRAN II**.

## METHOD OF CALCULATION

(Taken from the "Calculation of Ship Propulsion Shafting Bearing Reactions on an IBM 650 Computer" written by Edward T. Aptkowiak)

"Although the texts on indeterminate structures illustrate various devices for handling continuous beams on multiple supports, such as Hardy Cross or Relaxation Method, Three Moment Equations, etc., the large memory capacity and speed of a digital computer permits a more 'classical' approach. This approach is based on a direct evaluation of the relationship of the beam load (w) to the deflection ( $\delta$ ).

$$EI \frac{d^4 \delta}{dx^4} = W$$

"Therefore, successive integrations of the load-stiffness diagram will yield shear, moment, slope and deflection. However, in order to obtain zero deflection at each support, the correct reactions would have to be included in the load diagram prior to the integration. In the shafting problem, the reactions at each support are the unknowns.

"If the reactions are not included in the load diagram and it is assumed that the beam is held firmly at one end, the successive integrations will result in a deflection diagram similar to that shown in Figure 1 (a). Applying estimated reactions whose magnitudes are proportional to the deflection will yield a diagram with a smaller deflection, as shown in Figure 1 (b). Further approximations and successive integrations will converge to a zero deflection at the

supports, as shown in Figure 1 (c). At this point, the correct reaction has been applied.

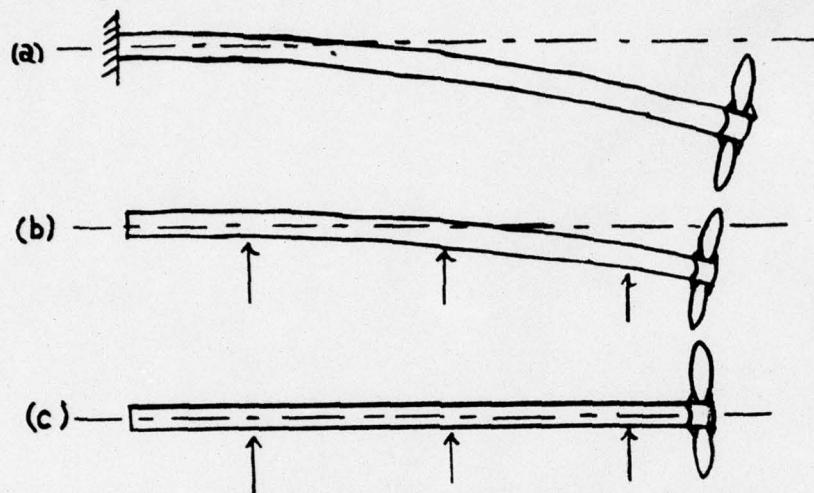


Figure 1 - Convergence of Shaft Deflection Curve to a Straight Line by Adding Support Reactions

"In order to apply this principle to practical use, some method of obtaining reaction estimates had to be devised. The method used is to determine the amount of reaction change produced by raising or lowering a bearing support a unit amount. This is also one of the final answers to our problem. These influence numbers are obtained by assuming the shaft has no weight and that a unit reaction is applied to one bearing. Successive integrations will then yield resulting deflections at all other bearing locations. By applying this unit reaction to each support in turn, a family of deflections will be obtained which can be substituted into a set

of equations (two more equations than there are number of support points), expressing the relationship of reactions and deflections. Solution of these equations will yield the 'influence numbers' necessary to the final solution of straight line reactions.

"Multiplying the influence numbers by the deflections obtained from integration of the unsupported, weighted (real) shaft, and summing the reaction changes for each bearing, the final straight line reactions will result. Applying this total reaction for each bearing to the load diagram and repeating the integration process, the deflection at each support will be zero, thus proving that the correct reaction has been applied. If the deflection is not zero, the entire process can be repeated until the bearing deflection becomes trivial."

## THEORY

Figure 2 shows a sample section of shaft with nomenclature as in the Notation. The programs compute moment of inertia and weight per unit length as follows:

Outer area

$$A_a = \pi/4 (d_a^2 - d_b^2)$$

Inner area

$$A_b = \pi/4 (d_b^2 - d_c^2)$$

Innermost area

$$A_c = \pi/4 d_c^2$$

Inertia of outer part

$$I_a = \pi/64 (d_a^4 - d_b^4)$$

Inertia of inner part

$$I_b = \pi/64 (d_b^4 - d_c^4)$$

Weight per unit length

$$A_a \rho_a + A_b \rho_b + A_c \rho_c - (A_a + A_b + A_c) \rho_d$$

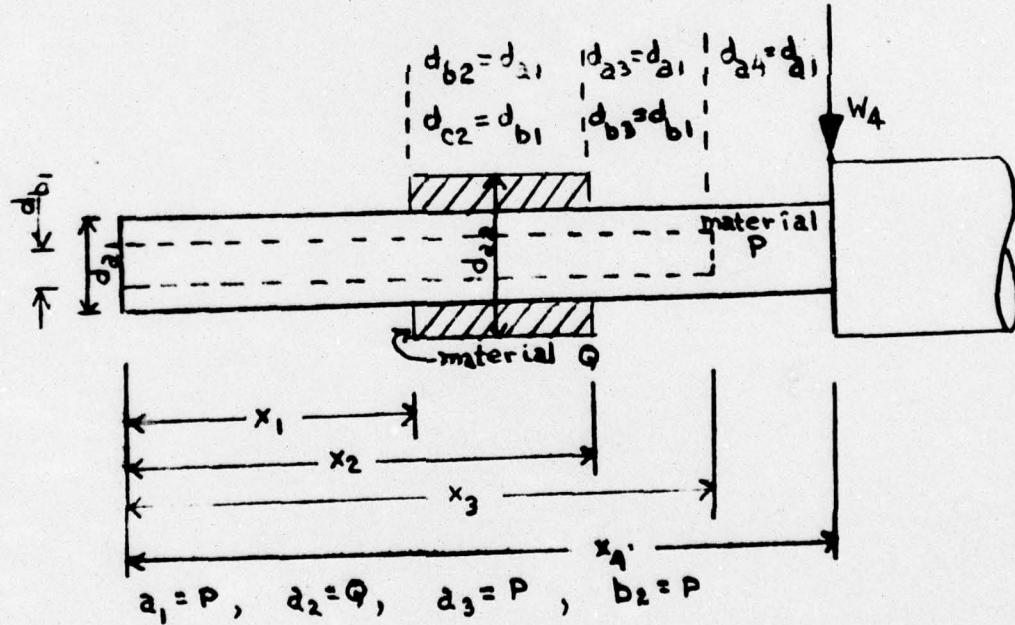


Figure 2 - Section of Shaft with Computational Inputs Labelled

where the first term (Material a) must be present in all cases; the second term (b) will be present for two materials; the third (c) is present only if the bore is filled with sand; and the fourth (d), which represents the upthrust of water, is present only if the shaft is wholly or partly immersed in water.

Consider a shaft of no weight but with the same stiffness as the real weighted shaft. If such a weightless shaft were on "straight line" bearings, there would be no reaction; however, if one of the bearings should be raised by 1 mil, forces would occur at each bearing.

These forces are the "influence numbers" which form an  $n \times n$  matrix where  $n$  is the number of bearings. The element in the  $i^{\text{th}}$  column and  $j^{\text{th}}$  row gives the force on Bearing  $i$  for a deflection of 1 mil at Bearing  $j$ .

Consider the weightless shaft acting as a cantilever as shown in (a) of Figure 3. When a unit force is applied at B, Section AB will be

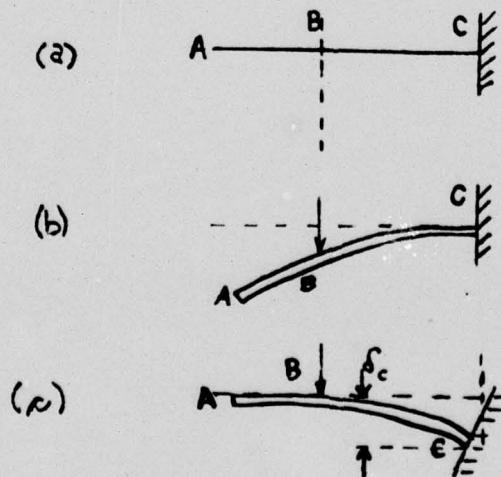


Figure 3 - Force Applied to a Weightless Cantilevered Beam

straight, but inclined at an angle to the horizontal (b). There is an advantage to assuming that Section AB remains horizontal with the wall moved (c), using AB as the reference axis.

Now consider the shear force, bending moment, slope, and deflection diagrams. According to the theory of beam deflection, these diagrams are related to one another by integration (see Figure 4).

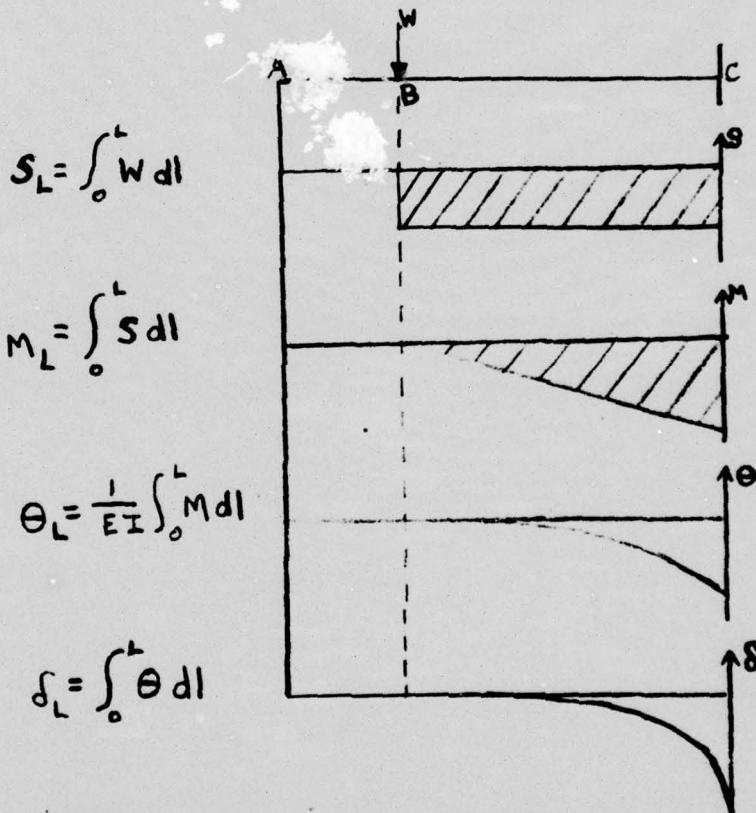


Figure 4 - Successive Integrations of a Load Stiffness Diagram

The result of a series of such integrations is summarized in tabular form by Table 1. Thus  $d_{24}$  is the deflection at Station 4 for a force of unity applied at Station 2.

TABLE I

Table of Deflections Resulting from Applying  
Individual Unit Reactions

Force Applied at Station Number:						Deflection at Station Number:					
1	2	3	4	5	6	1	2	3	4	5	6
1							$d_{12}$	$d_{13}$	$d_{14}$	$d_{15}$	$d_{16}$
	1							$d_{23}$	$d_{24}$	$d_{25}$	$d_{26}$
		1							$d_{34}$	$d_{35}$	$d_{36}$
			1							$d_{45}$	$d_{46}$
				1							$d_{56}$
					1						

If the beam Section AB is not considered to be horizontal or at zero slope, these deflections must be corrected as follows:

At A: add  $\Delta_o$

At B: add  $\Delta_o + \theta_o x_1$

At C: add  $\Delta_o + \theta_o x_2$  (see Figure 5).

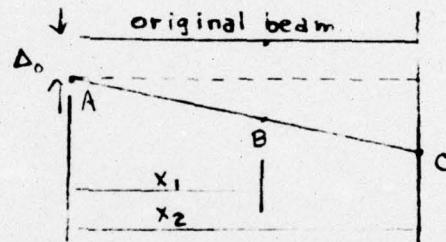


Figure 5 - Beam (Shaft) Displaced from Horizontal Reference Line

When unit reactions  $R_1, R_2, \dots R_n$  occur at support points 1, 2, ... n along the weightless shaft, the following equations apply:

$$\delta_1 = \Delta_o + \theta_o x_1$$

$$\delta_2 = \Delta_o + \theta_o x_2 + d_{12} R_1$$

$$\delta_n = \Delta_o + \theta_o + x_n + d_{1n} R_1 + d_{2n} R_2 + \dots + d_{(n-1)n} R_{(n-1)}$$

Two additional equations are required to solve this group; they may be found by considering the beam end C in Figure 5 as unfixed when it is

supported by reactions along its length. When acting as a multiply supported beam, this free end has no shear or moment, such that

$$0 = R_1 + R_2 + \dots + R_n$$

$$0 = x_1 R_1 + x_2 R_2 + \dots + x_n R_n$$

All these equations can therefore be put into a  $n+2$  equation square matrix form

$$\begin{array}{c|ccccc|c} \delta_1 & 1 & x_1 & 0 & 0 & \dots & \Delta_0 \\ \delta_2 & 1 & x_2 & d_{12} & 0 & \dots & \theta_0 \\ \delta_3 & = & 1 & x_3 & d_{13} & d_{23} & 0 & \dots & R_1 \\ \cdot & & \cdot & \cdot & \cdot & \cdot & \cdot & \cdot \\ \cdot & & \cdot & \cdot & \cdot & \cdot & \cdot & \cdot \\ \cdot & & \cdot & \cdot & \cdot & \cdot & \cdot & \cdot \\ \delta_n & & 1 & x_n & d_{1n} & d_{2n} & d_{3n} & \dots & \cdot \\ 0 & & 0 & 0 & 1 & 1 & 1 & \dots & \cdot \\ 0 & & 0 & 0 & x_1 & x_2 & x_3 & \dots & R_n \end{array}$$

representing the deflections for a given reaction. Inversion of this matrix gives the reactions for a given deflection, the reaction influence numbers. The columns which give deflection and slope condition now give slope and deflection influence numbers (i. e., the end slope and

the deflection for a given deflection at an intermediate point). Thus  $\alpha_{32}$  represents the reaction at Support 3 for a theoretical unit deflection at Bearing 2.

Assuming the initial slope and deflection are zero and that reactions at support points are zero (shaft cantilevered at one end), the end shear ( $V_1$ ) and end moment ( $M_1$ ) of the weighted shaft are calculated. These results are used to modify the first ( $R_1$ ) and last ( $R_n$ ) reactions, so that  $V_1$  and  $M_1$  then approach zero.

Consider the actual shaft with only two external bearings, held at the end to ensure no initial slope and deflection (see Figure 6), with total shaft weight  $W$ , total moment from the other end  $M$ , and total length  $L$ . (The convention assumed is that all downward forces are negative.)

$$\text{Then: } R_a + R_b = -W$$

$$(L-x_1) R_a + (L-x_n) R_b = -M$$

from which  $R_a$  and  $R_b$  are found. The new moments, slopes, and deflections can be found by considering the real weight shaft with concentrated loads.

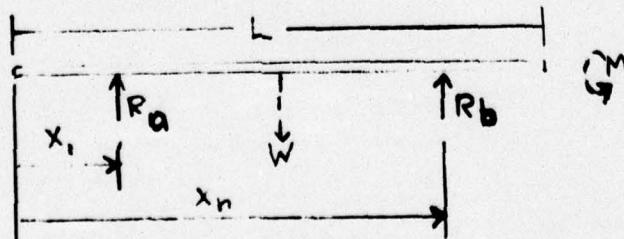


Figure 6 - Real Weighted Shaft with Only Two Bearings Present

The above discussion presents the solution to the two-bearing problem. Then, by using the influence numbers, the effect on the reactions when all the bearings are moved to the correct position can be found;  $\Delta_0$  and  $\theta_0$  are modified at this time.

The actual answers from the inversion will not be exact, but repeated entry into the deflection integration routines will give corrected values of the deflection for all bearings. Several of these weighted integrations may be required to obtain results within the required margin.

## MGE2 - STRAIGHT-LINE BEARINGS

### PROGRAM DESCRIPTION

To calculate the characteristics of a shaft with all supports on a straight line as outlined in "Method of Calculation," the shafting system must be divided into a number of stations, subject to the following restrictions:

1. Total number of stations must not exceed 400.
2. Total number of supports must not exceed 22.
3. Each change in cross-section diameter, each bearing location, each concentrated load, and the beginning of each immersion requires a new station.
4. Although the length of each station is arbitrary, there should be enough of these stations to provide sufficient abscissa points for plotting shear, moment, slope, and deflection diagrams, if desired.
5. All stations (except the last) must have nonzero diameter and material. The last data card is not considered a section; it serves to specify the total length of the shafting system.
6. Bearing may not occur at the first or at the last station.
7. Concentrated loads should not appear at bearing locations since calculated bearing-reaction values will overwrite the concentrated loads. Add an additional shaft section with a 0.100-inch, or even a 0.0001-inch, separation.

The program is written in a general manner and provides for the following variables:

1. Material of shaft
2. Shaft in air or water
3. Shaft solid or hollow
4. Sand in bore of hollow shaft

The specific moduli and densities in the program are:

Code	Material	Density (lb/cu in.)	Modulus (lb/sq in.)
1	Steel	.28355	$30 \times 10^6$
2	Bronze	.31399	$15 \times 10^6$
6	Sand	.0636	
7	Salt water	.03705	

If materials used in a specific shaft have constants quite different from the above, additional values may be added.

Slight changes in diameter may be ignored when the effect on weight and stiffness of the shaft is negligible. The average diameter of the propeller taper is used.

Loads acting downward will be negative. In most cases, reactions will be positive. However, in some instances where several bearings are close together, one bearing may indicate a negative reaction for the straight-line condition.

The weight of the propeller is applied as a concentrated load at its center of gravity, if known; otherwise, the weight is considered to

act at the middle of the tapered section. The dry weight of an immersed propeller may be reduced to take into account the buoyant effect of water by using the relationship

$$W(\text{water}) = W(\text{air}) * \frac{D_p - D_w}{D_p}$$

where  $D_p$  is the density of the propeller material and  $D_w$  is the density of the water.

Bearing reactions are assumed to act at points in the middle of the fore and aft ends of the bearings. However, in the case of a relatively long bearing such as a stern tube, it may be assumed that the load is concentrated one shaft diameter forward of the aft end of the bearing. For a more detailed study, support points at several positions along a bearing may be assumed.

The program gives the magnitude of all bearing reactions, assuming all bearings on a straight line. It prints slope and deflection influence numbers, which represent the amount of change in all bearing loads resulting from raising a particular bearing 0.001 in. from the straight line. Values of shear, moment, slope, deflection, weight (in pounds per inches), and stiffness (in terms of  $\frac{1}{EI}$ ) are given for each station. The total weight of the shaft and the location of the center of gravity are also printed.

The criteria for determining zero deflection at a bearing and the absence of shear force or moment at the free end are listed below:

1. Deflection at a bearing no greater than 0.001 in.
2. Shear force at free end less than 10 lb.
3. Bending moment at free end less than 100 in.-lb.
4. A maximum of four iterations on the deflection check.
5. A maximum of four iterations on the shear and moment checks.

The following error printouts occur after unrecoverable errors have been detected. The program then transfers to next data case.

The printout TOO MANY ITERATIONS DEFL XXXX MOMENT XXXX occurs when four iterations through DEFLN and BEAM have failed to meet ~~terminal~~ deflection, bending moment, and shear force criteria. The current results are then accepted.

The printout STATION DISTANCE ERROR occurs when stations are not input in ascending order of distance from Station 1. Case is terminated.

The printout SINGULAR INFLUENCE NUMBERS occurs if matrix is singular. Since it is indicative of incompatible data, case is terminated.

## OPERATING INSTRUCTIONS

1. The program run with 7090 IBSYS Version 13 includes the following cards:

\$JOB	
\$EXECUTE	IBJOB
\$IBJOB	FIOCS

decks	MGE2
	RED2
	BEAM
	DEFL
	INOU
	INFN
	AM MAT2
	AM DPAF

### \$DATA

MGE2 heading card for input case 1  
One card per station for input case 1  
One card for each constant change (omit if no material  
constant changes)  
Sentinel card with punch in column 2  
Additional cases of data, if called for by sentinel

Final sentinel has 9- or 7-punch in column 2  
7 END OF FILE

2. Output of five or more pages per case is written on SYSPU1 for program control printing.

At NSRDC, when compiled with plot option, control cards

\$ATTACH	B9
\$AS	SYSLB4

are inserted before \$ EXECUTE card, and plots for SC 4020 may be

prepared on **SYSLB4**. Deck **GRAP** must also be included before  
**\$DATA** card.

3. Total time for **IBSYS** compile, load, and execute of six varied cases was 1.8 min. Since the load time for retrieval of binary program deck from master instruction reel with **\$IEDIT** is 1 min, it is obviously advantageous to run multiple cases.

4. No sense switches, sense lights, or scratch files are used by the program. Memory requirement (including **I/O** subroutines) 19,400. For smaller computer, dimensions could be revised.

5. The program run on **LARC** includes:

Data cards for Program **MGE2**, followed by six cards with **END OF TAPE** punched in columns 1-12, are converted to tape and ready for mounting on Unit 11.

Object code tape containing instructions for routine

**MGE2**  
**READ2**  
**BEAM**  
**DEFL**  
**INOU**  
**INFN**  
**AM MAT2L**

is mounted on Unit 13.

Output is written on Tape 20 for 1/1 **LSC** loop printing.

## SC 4020 PLOTS

An option for SC 4020 graphic output may be used at NSRDC on 7090 or LARC. Card MGE2 0164 (or MGE5 0119) is changed from

981    CONTINUE    to    981    CALL GRAPH

The graph routine is listed in Appendix A.

The two sets of plots made for each case are moment and deflection versus station distance. If the total number of stations is less than 99, one frame is produced for each graph. For larger numbers of stations, a fixed station distance scale of 450 ft/frame results in 2 to 21 frames for each graph.

The ordinate versus abscissa is plotted as a continuous line with bearing stations further identified by X. See Appendix A for sample output.

## SHAFT ARRANGEMENT

Figure 7 shows a typical line shaft dimensioned for preparation of input data. The sketch should be made to some appropriate scale, using information from arrangement, assembly, and detailed drawings of low speed gear and shaft. The relationship of the components can then be readily observed.

1. The total number of stations must not exceed 400 and the total number of support points must not exceed 22.

2. Station 1 is the forward end of the shaft and all other stations are located in terms of their distance from Station 1. A station must be initiated at each support point, at each concentrated load, and at each significant change in cross-section diameter. Concentrated loads should not appear at bearing locations; an additional station with 0.001- or 0.0001-in. separation may be used (see note at end of paragraph). To reduce the number of stations, slight changes in diameters may be ignored or combined when their effect on the weight and stiffness of the shaft is negligible. Thus, in Figure 7, since the journal sections were only 1/4 in. wider than the shaft, they were considered to be the same diameter as the shaft. Also the average diameter of the tapered propeller section was used. Note that, if desired, the additional weight of journal sections may be compensated for without increasing the number of stations by adding the weight as concentrated load at the center of the

bearing, but such a load would not be included in the bearing reactions given as output. All concentrated weights, however, are included in the total weight of the shaft.

3. Where the thrust collar is forward of the low speed gear and not integral, its weight is treated as a concentrated load, since it does not add significantly to the stiffness of the system. In Figure 7, the thrust bearing is aft of the low speed gear and the thrust collar is integral with the shaft; therefore, it is treated as part of the shaft.

4. a. Since the gear is not a solid section (rim, webs, etc.), an equivalent outside diameter must be used to obtain its proper lateral stiffness. The outside diameter of the hub section may be used as the equivalent outside diameter.

b. The difference between the total weight of the actual low speed gear and shaft assembly and the calculated weight of the equivalent assembly is applied as a concentrated load on this section so that the total weight will be correct.

c. In Figure 7, this difference is applied as one concentrated load at the centerline of the gear, midway between fore and aft bearings. Present practice is to divide the concentrated load by the number of webs, and to apply these equal loads at the points where the webs meet the hub. In most cases, either method may be used.

5. Bearing reactions are assumed to act at points midway between the fore and aft ends of each bearing. In the case of long bearings (such as a stern tube bearing), it may be assumed that the load is concentrated one shaft diameter forward of the aft end of the bearing. For a more exact detailed study, support points at several positions along a bearing may be assumed.

6. If the shaft is to be studied with the ship waterborne, a note should be made on the sketch (Figure 7) to indicate what portion of the shaft is to be immersed. A station must be initiated at the beginning of the immersion.

7. The weight of the propeller is applied as a concentrated load at its center of gravity, if known; otherwise, the weight is considered to act at the middle of the tapered section. The dry weight of an immersed propeller should be reduced to take into account the buoyancy effect of salt water by the relationship

$$\text{Weight (water)} = \text{Weight (air)} \times \frac{\text{Density (prop)} - \text{Density (water)}}{\text{Density (prop)}}$$

For bronze with a density of 0.31399 lb/cu in. and salt water with a density of 0.03705 lb/cu in., the multiplicative factor would be 0.882.

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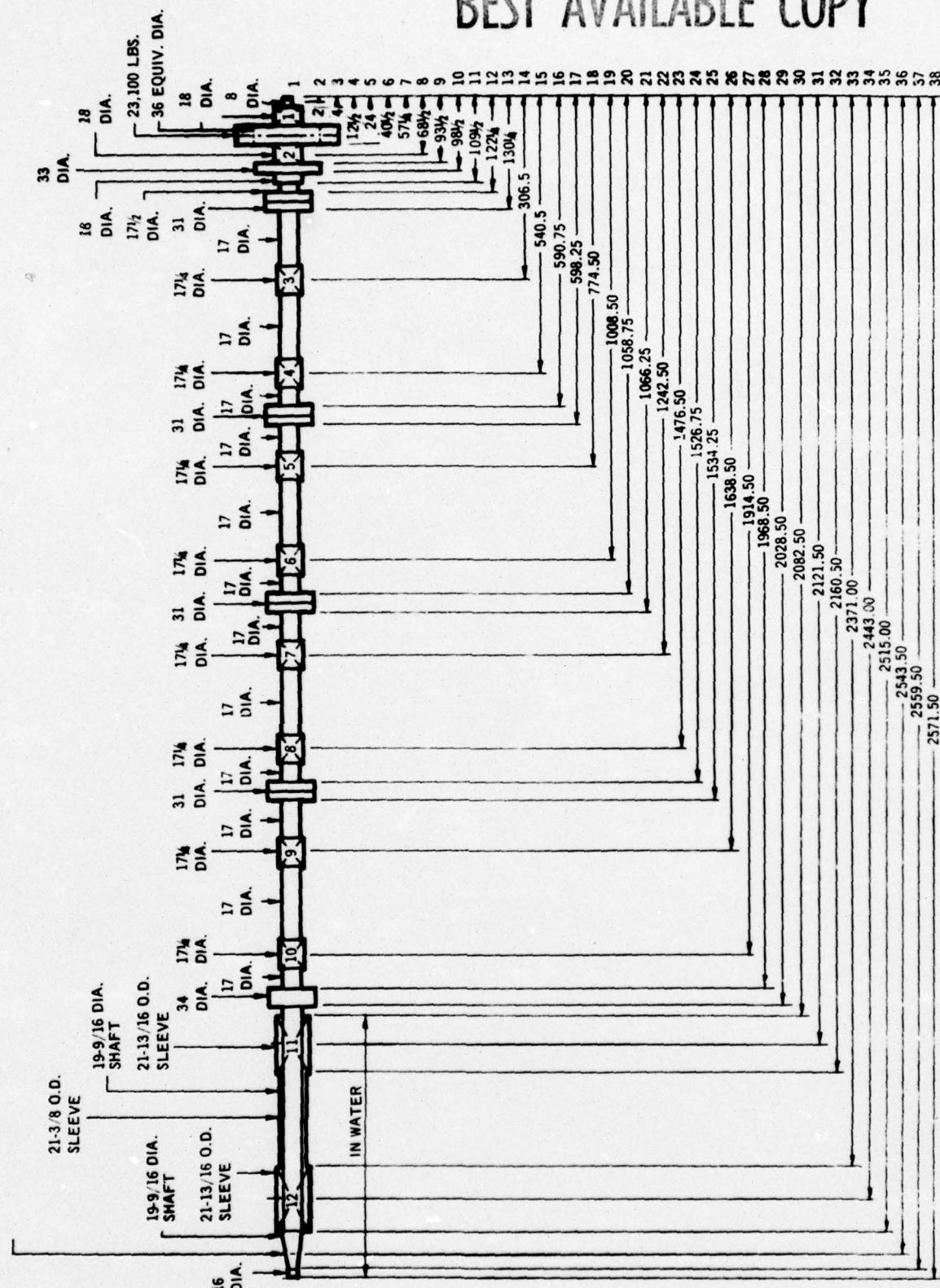


Figure 7 - Shafting Arrangement Dimensions for Computer Program

TOTAL WT. OF L.S. GEAR & SHAFT - 40,500 LBS. SHAFT ONLY - 11.05 LBS. ESTIMATED EQUIV. CYA. OF HUB FOR LATERAL STIFFNESS 36 O.D.

## DATA PREPARATION

1. **MGE2 Title Card:** Columns 1-72 alphanumeric information to identify the case.

2. One card for each station (maximum of 400) in accordance with **FORMAT (I3, 5F12.4, 2I2, 2I1).**

### Column No. Explanation

1-3	Station number right justified ( $\Delta\Delta 1, \Delta\Delta 2, \dots, 105, 106$ , etc.). Last station must have 9 in column 1 as sentinel.
*4-15	Distance of beginning of station from Station 1, in inches.
*16-27	Outer diameters, in inches.
*28-39	Second diameter, in inches. Inner diameters of bushing or sleeve if used, or diameters or bore if hollow shaft.
*40-51	Third diameter, in inches. Diameter of bore in a hollow shaft which also has bushing or sleeve.
*52-63	Concentrated weight (if present) minus values for downward weight.
64 blank	
65	**Material of outer diameters { 1, if steel 2, if bronze
66 blank	
67	**Material of inner diameter { 1, if steel 2, if bronze
68	Bearing position - blank, if no support; 1, if bearing present.
69	1, if shaft in water; blank, if in air.
70	1, if sand bore; blank, if no sand.

\* The above numbers may be punched anywhere in field, and the decimal point must be punched.

\*\* If material is other than steel or bronze, new constants for density and modulus of elasticity must be given.

3. One card for each new material or change of density and modulus of elasticity using **FORMAT (2I2, 2F12, 2)**. (Omit if no material constant changes.)

Column No. Explanation

2	Code for action to be taken:
1	- new density only
2	- new modulus only
3	- new density and modulus
4	- set to punch influence numbers (not activated in current program)
4	Code for material:
1	- steel
2	- bronze
6	- sand
7	- water
3, 4, 5	- for new materials
5-16	New density if 1 or 3 in column 2 New modulus if 2 in column 2
17-28	New modulus if 3 in column 2

4. End of Case sentinel card (I2).

Column 2 Explanation

0 or blank	End last case, no graphs.
7	End last case after graphing
8	Graph, then more cases follow.
9	More cases follow, no graphs.
5, 6	Same as 0.

## MEG5 - BEARINGS RAISED OR LOWERED

### PROGRAM DESCRIPTION

The table of influence numbers obtained from MGE2 enables the calculation of reactions when certain bearings are moved vertically off the straight line. However, MGE5 must be used to find the shear force, being moment, slope, and deflection at each station caused by raising or lowering certain bearings.

When a study of shaft characteristics from MGE2 suggests that a better alignment could be achieved by raising or lowering certain bearings, MGE5 should be run to determine whether the repositioning imposes excessive shear forces or bending moments on the shaft.

The same general computational procedure is used for both MGE5 and MGE2. However, since the influence numbers and weight and stiffness factors of the shaft system are not affected by changing the elevation of bearings, the output of this MGE5 program does not list these factors. It gives instead a single page of shear, moment, slope, deflection, and bearing reactions.

Restrictions on input are the same as those for MGE2.

## OPERATING INSTRUCTIONS

1. The program run with 7090 IBSYS Version 13 includes:

\$JOB	
\$EXECUTE	IBJOB
\$IBJOB	FIOCS

decks	MGE5
	RED5
	Beam and rest of decks same as MGE2

### \$DATA

MGE5 heading card for input case 1  
One to give bearing change cards  
MGE2 heading card for input case 1  
One card per station for input case 1  
One card for each constant change (omit if no material  
constant changes)  
Sentinel card with column 2 punched  
Additional sets of input data if called for by sentinel  
.  
.  
.  
Final sentinel has 9-or 7-punch in column 2.  
7 END OF FILE

2. Output of one page per case is written on SYSOU1 for program control printing. Plot option is as in MGE2.

3. Execution time is similar to MGE2.

4. The program run on LARC includes:

Data cards for Program MGE5, followed by six cards with  
END OF TAPE punched in columns 1-12, are converted to tape for  
mounting on Unit 11.

**Object code tape containing instructions for routines**

**MGE5  
READ5  
BEAM  
DEFL  
INOU  
INFN  
AM MAT2L**

**is mounted on Unit 13.**

**Output is written on Tape 20 for 1/1 LSC loop printing.**

## DATA PREPARATION

1. **MGE5 Title Card:** Columns 1-72 alphameric information to identify how case differs from similar MGE2 run.
2. One to five bearing change cards using **FORMAT (I1, 5F11.8).**

<u>Column No.</u>	<u>Explanation</u>
1	Blank or 0, if not last card; 9, if last change card.
2-12	Relocation of bearing 1 from straight line.
13-23	Relocation of bearing 2 from straight line.
24-34	Relocation of bearing 3 from straight line.
35-45	Relocation of bearing 4 from straight line.
46-56	Relocation of bearing 5 from straight line.

Next card would contain relocation for next five bearings. Values are given in inches; location of bearing may be punched anywhere in field and the decimal point must be punched.

Plus value is bearing above the line; minus value is below.

3. A complete set of MGE2 input cards, including case sentinel.

## ACKNOWLEDGMENTS

These programs are adaptations of shafting systems programs written originally for IBM 650 by Mr. Edward Antkowiak of the Boston Naval Shipyard; his assistance in preparing this version is appreciated. Much of the coding of an expanded shafting program for IBM 704, done by Mr. Edgar H. Sibley and others at the General Electric Lynn Digital Computer Section, is included within this program. Mr. Ralph E. Wolfe of the Boston Naval Shipyard contributed greatly to the theoretical approach to this calculation and originated the concept of obtaining the influence numbers by integration of a "weightless" shaft. Mr. Frank Zaher of Naval Ship Systems Command and Mr. Edward Ryan, formerly of New York Naval Shipyard, made suggestions which have been incorporated in the final program.

Other versions of the shafting program, written at Boston Naval Shipyard, are also available for IBM 1620 and Burroughs Datatron 205.

## APPENDIX A

## MGF2 = PROGRAM LISTING

BRG. NO.	SLOPE	DEFLECTION
2	3	MGE20037
1010	FORMAT(135,F30.7,F30.8)	MGE20038
1030	FORMAT(1H120X,12A6//)	MGE20039
1031	FORMAT(///40X,35H)	MGE20040
1	110H STATION	MGE20041
1	SLOPE	MGE20042
2	113H NO.	MGE20043
1	(RADIAN)	MGE20044
1032	FORMAT(// 40X,44H)	MGE20045
1	11CH STATION	MGE20046
1	STIFFNESS(1/EI)	MGE20047
4	111H NO.	MGE20048
1	(X0.000000000001)	MGE20049
1035	FORMAT(// 40X,44H)	MGE20050
1	1 / F14.1,10F10.1 )	MGE20051
1036	FORMAT(1H1 40X, 42H *** SHAFTING SYSTEM	MGE20052
1	20X,12A6//52X,14H INPUT DATA //)	MGE20053
1037	FORMAT(F14.1,10F10.1 )	MGE20054
1038	FORMAT(// 8X, 70HTOTAL SHAFT	MGE20055
	INCENTRATED LOADS) = F11.2,7H	MGE20056
2	/80H DISTANCE OF CENTER /	MGE20057
3	STATION NO. 1 = F10.4,7H	MGE20058
	INCH )	MGE20059
1050	FORMAT(19,-3PF21.5,F19.3,OPF20.7,F20.7,F18.1)	MGE20060
1090	FORMAT(19,F20.4,F20.4,	MGE20061
C	DENSITY AND MODULUS FOR STEEL, BRONZE	MGE20062
1221	YMAT(1)=30000000.0	MGE20063
	YMAT(2)= 15000000.0	MGE20064
	DENMAT(1)=-0.28355	MGE20065
	DENMAT(2)=-0.31399	MGE20066
C	CLEAR STORAGES TO ZERO INITIALLY	MGE20067
	DO 2001 ISET=1,25	MGE20068
	DO 2000 JSET = 1,25	MGE20069
2000	BNFLUI(JSET,ISET) = 0.0	MGE20070
2001	CONOT(ISET) = 0.0	MGE20071
	DO 2003 ISET=1,1620	MGE20072

A. 2

```

MGE20073
MGE20074
MGE20075
MGE20076
MGE20077
MGE20078
MGE20079
MGE20080
MGE20081
MGE20082
MGE20083
MGE20084
MGE20085
MGE20086
MGE20087
MGE20088
MGE20089
MGE20090
MGE20091
MGE20092
MGE20093
MGE20094
MGE20095
MGE20096
MGE20097
MGE20098
MGE20099
MGE20100
MGE20101
MGE20102
MGE20103
MGE20104
MGE20105
MGE20106
MGE20107
MGE20108

2003 BMTAB(ISET)=C.0
2003 SFTAB(ISET)=C.0
DO 2004 ISET=1,401
2004 CANOT(ISET)=0.0
NIB=1
IERROR = 1
READ (5,1) TITL2
WRITE (6,1036) TITL2
WRITE (6,20)
CALL READIN
IF(IERROR-1) 57,57,560
57 CALL INFNOS
62 WRITE(6,1030) TITL2
CALL INOUT
WRITE(6,1000)
WRITE(6,1010)(NO(J),(BNFLU(JA,J),JA=24,25),J=1,IBRS)
IF(IERROR-1) 65,65,560
65 CALL DEFLN
I2=4*N+4
WBAR=SFTAB(I2)
XBAR= DISTL(N+1) -BMTAB(I2)/SFTAB(I2)
CALL BEAM
CALL DEFLN
K=N+1
230 WRITE(6,1030) TITL2
WRITE(6,24)
KTEST = 0
KTES2=0
210 DO 300 I1=1,IBRS
IBSR=IBTAB(I1)
DO 250 I2=1,IBRS
IASR=IBTAB(I2)
CONWT(IBSR)=DEF(IASR)*BNFLU(I1,I3)*(-1000.0) +CONWT(IBSR)
THETA(1)= THETA(1)-(DEF(IBSR)*BNFLU(25,I1))
300 DEF(1) =DEF(1) - ( DEF(IBSR)* BNFLU(24,I1) )
979 CALL DEFLN

```

```

DO 400 I=1,IBRS
J=1BTAB(I)
IF (ABS (DEF(J))- .001)400,400,445
400  CONTINUE
        IF(KTEST-.4) 410, 450, 450
410  IF(ABS(1BTAB(I2))-100.)1420,222,222
420  IF(ABS(1SFTAB(I2))-10.)1500,222,222
222  KTEST = KTEST +
CALL BEAM
GO TO 979
445  KTES2=KTES2+1
        IF (KTES2-.4) 210, 450, 450
450  WRITE(6,451) KTES2,KTEST
451  FORMAT(27H0TO MANY ITERATIONS - DEF1 14, 9H MOMENT 14)
500  DO 515 I=1,K
        DIST(I)= 0.0
        IF (STIFX(I))515,515,514
514  DIST(I)=1.E12/STIFX(I)
515  CONTINUE
800  DO 825 I=1,IERs
        J=1BTAB(I)
        CON(I)=CONWT(I)
        CANOT(I)=CONCT(I)
        IF (IBRS-.1) 350,350,351
350  K2 =IBRS
        GO TO 310
351  K2 = 11
310  CONTINUE
320  WRITE(6,203)
        DO 322 J=1,IBRS
322  WRITE(6,200)NO(J),(BNFLU(I,J)), I=1,K2)
        WRITE (6,1035)
        WRITE (6,1037) (CONOT(I),I=1,K2)
352  IF (IBRS-.1)517,517,357
357  WRITE (6,205)
        DO 358 J=1,IBRS

```

```

358 WRITE (6,200) NO(J), (BNFLU(I,J), I=12,1BRS)
      WRITE (6,1035)
      WRITE (6,1037) (CONOT(I), I=12,1BRS)
517  CONTINUE
540  WRITE (6,1030) TITL2
      WRITE (6,1031)
      DO 545 I=1,K
      IB = I+I
      IA = IB+IB
545  WRITE (6,1050) NO(I), SFTAB(IA), BMTAB(IA), THETA(IB-1), DEF(I).
      1 CANOT(I)
      WRITE (6,1030) TITL2
      WRITE (6,1032)
547  WRITE (6,1090) (NO(I), DISTL(I), WTS(I), CONWT(I), LIBRG(I),
      I I=1,K)
      WRITE (6,1038) WBAR, XBAR
      IXM = IXM
      IF(IXM)1222,1222,980
      980  GO TO(1222,1222,1222,1222,981,981,1221), IXM
      981  CALL GRAPH
      560  IF(IXM-7)1222,1222,1221
      1222  CONTINUE
      WRITE (6,1036)
      STOP
      END

```

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```

51BFTC RED2 DECK
C READIN MGE2
C SUBROUTINE READIN
C KEY FOR IXM SENTINEL
C
C BLANK ,N SINGLE CASE, LAST CASE - NO PLOT
C IXM - 1 NEW DENSITY
C 2 NEW MODULUS
C 3 NEW DENSITY AND MODULUS
C 4 MULTIPLE WT RUN - SPEC CASE
C 5,6 SAME AS ,0
C 7 PLOT SINGLE CASE
C 8 PLOT THEN MULTIPLE CASES
C 9 MULTIPLE CASES - ANOTHER FOLLOWS - NO PLOT
C VARIABLE NAMES USED IN READIN DO NOT MATCH REST OF PROGRAM
C
DIMENSION A(401), B(401), C(401), D(401), E(401), I(401), J(401),
1K(401), L(401), IS(401), H( 7), P( 7), DISTT(401), BMTAB(1620),
2THETA(802), DEF(401), BNFLU(25,25), DIBRG(25), IBTAB(25), SFTAB(1620),
3TITLE(12),
NO(400)
COMMON N,NO,A,B,C,D,E,I,J,K,L,IS,H,P,DISTT,BMTAB,THETA,DEF,
IBNFLU,DIBRG,IBTAB,
2 IBRS,SFTAB,12,IERRO, TITL2,IXM
DIMENSION NS(50)
COMMON SWAT,NS,SYM
FORMAT(13.5F12.4,212,311)
10 FORMAT(212,2F12.2)
15 FORMAT(17,4F14.4,F14.2,216,18,16)
20 FORMAT(25HO STATION DISTANCE ERROR
90 FORMAT(2413)
91 FORMAT(2413)
P(6)=-0.0636
P(7)=-0.03705
DO 40 N=1,400
22 READ(5,10)NO(N),A(N),B(N),C(N),D(N),E(N),I(N),J(N),K(N),L(N),IS(N)
IF( NO(N)-900)40,40,45
40 CONTINUE
45 NO(N) = NO(N) -900
51 WRITE(6,20)(NO(11),A(11),B(11),C(11),D(11),E(11),I(11),
RED20002
RED20003
RED20004
RED20005
RED20006
RED20007
RED20008
RED20009
RED20010
RED20011
RED20012
RED20013
RED20014
RED20016
RED20017
RED20018
RED20019
RED20020
RED20021
RED20022
RED20023
RED20024
RED20025
RED20026
RED20027
RED20028
RED20029
RED20030
RED20031
RED20032
RED20033
RED20034
RED20035
RED20036
RED20037

```

```

1J(11),K(11),L(11),IS(11),II=1,N)
55 PI=3.14159265 RED20038
      N = N-1 RED20039
24 READ (5,15) IXM,IYM,AVIT,DAVIT RED20040
      IF(IXM) 36,36,27 RED20041
      GO TO (29,25,28,81,36,36,36,36),IXM RED20042
27 H(IYM)=DAVIT RED20043
28 P(IYM)=AVIT RED20044
29 GO TO 24 RED20045
30 H(IYM)=AVIT RED20046
      GO TO 24 RED20047
31 SWAT=AVIT RED20048
      READ (5,91) (NS(I3),I3=1,IYM) OPTION NOT ALLOWED IN CURRENT
32 DO 79 I3=1,N RED20049
      DISTT(I3)=(A(I3+1)-A(I3))*.25 RED20050
      IF(DISTT(I3)>82.56,56
82 WRITE(6,90)NO(I3) RED20051
      TERROR = 2 RED20052
      GO TO 80 RED20053
      AREA1=PI*(B(I3)**2-C(I3)**2)/4.0 RED20054
      AMI1=PI*(B(I3)**4-C(I3)**4)/64.0 RED20055
      IMAT=I(I3) RED20056
      WT1=AREA1*P(IMAT) RED20057
      STIF1=H(IMAT)*AMI1 RED20058
      ST=STIF1 RED20059
      WAIT=WT1 RED20060
      IF(J(I3)>65,66,65 RED20061
      AREA2=PI*(C(I3)**2-D(I3)**2)/4.0 RED20062
      AMI2=PI*(C(I3)**4-D(I3)**4)/64.0 RED20063
      JMAT=J(I3) RED20064
      WT2=AREA2*P(JMAT) RED20065
      STIF2=H(JMAT)*AMI2 RED20066
      ST=STIF1+STIF2 RED20067
      WAIT=WT1+WT2 RED20068
      IF(L(I3)>70,75,70 RED20069
      AREA3=PI*(B(I3)**2)/4.0 RED20070
      IF(L(I3)>75,70,70 RED20071
      AREA3=PI*(B(I3)**4)/4.0 RED20072
      IF(L(I3)>70,75,70 RED20073
      AREA3=PI*(B(I3)**2)/4.0

```

```
WT3=AREA3*P(7)
WAIT=WAIT-WT3
75 IF(IIS(13))77,78,77
77 IF(D(13))68,69,68
69 WT4=(PI*C(13)**2/4.0)*P(6)
      GO TO 85
68  WT4=(PI*D(13)**2/4.0)*P(6)
85  WAIT=WAIT+WT4
78  D(13)=WAIT
     C(13)=ST
     CONTINUE
80  RETURN
     END

RED20074
RED20075
RED20076
RED20077
RED20078
RED20079
RED20080
RED20081
RED20082
RED20083
RED20084
RED20085
RED20086
```

```

SIBFTC DEFL DEFLN
  SUBROUTINE DEFLN
    C
    DEFLECTION FOR MGE2, MGE5
    DIMENSION DISTL(401),DIA(401),STIFX(401),WTS(401),CONWT(401),
    1IM(401),JM(401),IBRG(401),IWATR(401),IS(401),YMAT(7),DENMAT(7),
    2DISTT(401),BMTAB(1620),THETA(802),DEF(401),BNFLU(25,25),DIBRG(25)
    3,IBTAB(25),SFTAB(1620),TITL2(12),NO(400)
    COMMON N,NO,DISTL,DIA,STIFX,WTS,CONWT,IM,JM,IBRG,
    1 IWATR,IS,YMAT,DENMAT,DISTT,BMTAB,THETA,DEF,BNFLU,DIBRG,IBTAB,
    2 IBRS,SFTAB,I2,ERROR, TITL2,IXM
    DIMENSION NS(50)
    COMMON SWAT,NS,IYM
    DO 2 I=1,6
    SFTAB(I)=0.0
    2 BMTAB(I)=0.0
    SFTAB(4)=CONWT(1)
    5 DO 40 L=1,N
    5 I=4*L
    10 DO 20 J=1,4
    MA=I+J
    SFTAB(MA)=SFTAB(MA-1)+(WTS(L)*DISTT(L))
    20 BMTAB(MA)=(SFTAB(MA-1)+SFTAB(MA))/2.*DISTT(L)+BMTAB(MA-1)
    14 SFTAB(MA)=SFTAB(MA)+CONWT(L+1)
    40 CONTINUE
    DO 30 M=1,N
    IK = M+M
    I = IK+IK
    THETA(IK) =DISTT(M)/3.0*(BMTAB(I)+BMTAB(I+1)+BMTAB(I+2)+(4.0*BMTAB(I+1))/
    1STIFX(M)+THETA(IK-1))
    THETA(IK+1) = DISTT(M)/3.0*(BMTAB(I+2)+BMTAB(I+4)+(4.0*BMTAB(I+3))/
    1) /STIFX(M)+THETA(IK)
    30 DEF(M+1) =2.0/3.0*DISTT(M)*(THETA(IK+1)+THETA(IK-1)+(4.0*THETA(IK)*DEF(IK))
    1 )+DEF(M)
    RETURN
    END

```

```

S1BFTC BEAM2 DECK
      SUBROUTINE FOR MGE2 AND MGE5
C
      BEAM SUBROUTINE FOR MGE2 AND MGE5
      COMMON N,NO,DISTL,DIA,STIFX,WTS,CONWT,IM,JM,IBRG,
      1 IWATR,IS,YMAT,DENMAT,DISTT,BMTAB,THETA,DEF,BNFLU,DIBRG,IBTAB,
      2 IBRS,SFTAB,I2,ERROR, TITL2,IXM
      DIMENSION DISTL(401),DIA(401),STIFX(401),WTS(401),CONWT(401),
      1 IM(401),JM(401),IBRG(401),IWATR(401),IS(401),YMAT(7),DENMAT(7),
      2 DISTT(401), BMTAB(1620),THETA(802),DEF(401),BNFLU(25,25),DIBRG(25)IBAM010
      3,IBTAB(25), SFTAB(1620),TITL2(12),NO(400)
      DIMENSION NS(50)
      COMMON SWAT,NS,YM
      I1=IBTAB(1)
      BEAM0011
      BEAM0012
      BEAM0013
      BEAM0014
      BEAM0015
      BEAM0016
      BEAM0017
      BEAM0018
      BEAM0019
      BEAM0020
      BEAM0021

      ISEND = IBTAB(IBRS)
      CONWT(I1)=( BMTAB(I2)-(SFTAB(I2)*(DISTL(N+1)-DIBRG(IBRS)))/
      1(DIBRG(I1)-DIBRG(IBRS)) +CONWT(I1)
      CONWT(ISEND)=(BMTAB(I2)-(SFTAB(I2)*(DISTL(N+1)-DIBRG(I1)))/
      1(DIBRG(IBRS)-DIBRG(I1)) +CONWT(ISEND)
      RETURN
      END

```

```

$IBFTC INFN DECK
C INFLUENCE NUMBERS FOR MG2, MG5
SUBROUTINE INFNOS
DIMENSION DISTL(401),DIA(401),STIFX(401),WTS(401),CONWT(401),
1 IM(401),JM(401),IBRG(401),IWATR(401),IS(401),YMAT(7),DENMAT(7),
2 DISTT(401),BMTAB(1620),THETA(802),DEF(401),BNFLU(25,25),DIBRG(25),
3,IBTAB(25),SFTAB(1620),TITL2(12),NO(400)
COMMON N,NO,DISTL,DIA,STIFX,WTS,CONWT,IM,JM,IBRG,
1 IWATR,IS,YMAT,DENMAT,DISTT,BMTAB,THETA,DEF,BNFLU,DIBRG,IBTAB,
2 IBRS,SFTAB,12,ERROR, TITL2,IXM
DIMENSION NS(50)
COMMON SWAT,NS,IYM
N1=3
NTWO = N+N
NFOR = NTWO+NTWO
DO 99 I1=1,N
N2=2
IF (IBRG(I1)) 60,99,60
  DO 63 I3=1,N
  63 DEF(I3)=0.0
  DO 64 I32=1,NTWO
  64 THETA(I32)=0.0
  DO 65 I34=1,NFOR
  65 BMTAB(I34)=0.0
  DO 95 J1=11,N
  94 I4=4*J1
  DO 75 J2=1,4
  K1=I4+J2
  75 BMTAB(K1)=DISTT(J1)+BMTAB(K1-1)
  K2=2*J1
  THETA(K2)=DISTT(J1)*(BMTAB(K1-4)+BMTAB(K1-2)+(4.0*BMTAB(K1-3)))/(SINFN031
  1TIFX(J1)*2.0) +THETA(K2-1)
  THETA(K2+1)=DISTT(J1)*(BMTAB(K1)+BMTAB(K1-2)+(4.0*BMTAB(K1-1)))/(SINFN033
  1TIFX(J1)*2.0) +THETA(K2)
  95 DEF(J1)=(2.0/3.0)*DISTT(J1)*(THETA(K2+1)+THETA(K2-1)+(4.0*THETA(K2-1)+THETA(K2+1)+DEF(J1-1)
  1)) +DEF(J1-1)
  INFN001
  INFN003
  INFN002
  INFN004
  INFN005
  INFN006
  INFN007
  INFN008
  INFN009
  INFN010
  INFN011
  INFN012
  INFN013
  INFN014
  INFN015
  INFN016
  INFN017
  INFN018
  INFN019
  INFN020
  INFN021
  INFN022
  INFN023
  INFN024
  INFN025
  INFN026
  INFN027
  INFN028
  INFN029
  INFN030
  INFN031
  INFN032
  INFN033
  INFN034
  INFN035
  INFN036

```

```
DO 97 J3=1,N
  IF(1BRG(J3))96,97,96
96  BNFLU(N1,N2)=DEF(J3-1)
    N2=N2+1
97  CONTINUE
      N1=N1+1
99  CONTINUE
100 RETURN
END

INFN0037
INFN0038
INFN0039
INFN0040
INFN0041
INFN0042
INFN0043
INFN0044
INFN0045
```

```

1
1 NOU0002
1 NOU0003
1 NOU0004
1 NOU0005
1 NOU0006
1 NOU0007
1 NOU0008
1 NOU0009
1 NOU0010
1 NOU0011
1 NOU0012
1 NOU0013
1 NOU0014
1 NOU0015
1 NOU0016
1 NOU0017
1 NOU0018
1 NOU0019
1 NOU0020
1 NOU0021
1 NOU0022
1 NOU0023
1 NOU0024
1 NOU0025
1 NOU0026
1 NOU0027
1 NOU0028
1 NOU0029
1 NOU0030
1 NOU0031
1 NOU0032
1 NOU0033
1 NOU0034
1 NOU0035
1 NOU0036

SIBFTC INOU DECK
      SUBROUTINE INOUT      1
      IOUT FOR MGE2, MGE5
      C
      DIMENSION DISTL(401),DIA(401),STIFX(401),WTS(401),CONWT(401),
      1 JM(401),JM(401),IBRG(401),IWATR(401),IS(401),YMAT(7),DENMAT(7),
      2 DISTL(401),BNITAB(1620),THETA(802),DEF(401),BNFLU(25,25),DIBRG(25)
      3,IBTAB(25),SFTAB(1620),TITL2(12),NO(400)
      COMMON N,NO,CISTL,DIA,STIFX,WTS,CONWT,IM,JM,IBRG,
      1 IWATR,IS,YMAT,DENMAT,DISTT,BMTAB,THETA,DEF,BNFLU,DIBRG,IBTAB,
      2,IBRS,SFTAB,I2,IERRO, TITL2,IM
      DIMENSION NS(50)
      COMMON SWAT,NS,SYM
      IBRS = 0
      DO 2 11=1,22
      2 IBTAB(11) = 0.0
      DO 70 11=1,N
      IF (IBRG(11)) 70,70,65
      65 IBRS = IBRS +1
      IBTAB(1BRS) = 11
      DIBRG(1BRS) = DISTL(11)
      70 CONTINUE
      IBR1=IBRS+1
      IBR2=IBRS+2
      BNFLU(1,1) =0.0
      BNFLU(2,1) =0.0
      BNFLU(1,IBR2) = 0.0
      BNFLU(2,IBR2) = 0.0
      DO 102 J5=2,IBR1
      BNFLU(1,J5)=1.0
      BNFLU(2,J5)=DIBRG(J5-1)
      BNFLU(J5+1, 1) = DIBRG(J5-1)
      BNFLU(J5+1, 1) = 1.0
      102 CONTINUE
      CALL MATINV(BNFLU,IBR2,STOR,0,DETERM,1D)
      GO TO (221,610), 1D
      DO 600 K7= 1,IBRS
      231

```

```

NK7 = IBRS-K7+1
BNFLU(25,NK7) = BNFLU(NK7+1,2)
BNFLU(24,NK7) = BNFLU(NK7+1,1)
600 DO 236 K8 = 1,IBRS
DO 236 K7 = 1,IBRS
236 BNFLU(K7,K8) = BNFLU(K7+1,K8+2) * .001
550 CONTINUE
551 RETURN
C   ERROR SET FOR SINGULAR ARRAY
610 WRITE(6,611)
611 FORMAT(29HO SINGULAR INFLUENCE NUMBERS    //)
IERROR = 2
GO TO 551
END

```

```

$IBFTC MAT2 DECK
C MATRIX INVERSION WITH ACCOMPANYING SOLUTION OF LINEAR EQUATIONS
C INTERNAL DOUBLE PRECISION PIVOT METHOD
C NOVEMBER 1692 S GOOD DAVID TAYLOR MODEL BASIN AM MAT2
C
C SUBROUTINE MATINV(A,N1,B,M1,DETERM,ID)
C
C GENERAL FORM OF DIMENSION STATEMENT
C DIMENSION A( , ),B( , ),INDEX( ,3),A1( , ),B1( , )
C
C DIMENSION A(25,25),B( 1, 1),INDEX(25,3) ,A1(25,25),B1(1,1)
C EQUIVALENCE (IROW,JROW), (ICOLUMN,JCOLUMN), (AMAX, T, SWAP)
C EQUIVALENCE (T4,PIVOT1),(T5,PIVOT)
C
C INITIALIZATION
C
C N=N1
C M=M1
C 10 DETERM=1.0
C     D TERM1=0.0
C 15 DO 20 J=1,N
C     DO 17 I=1,N
C 17 A1(J,I) = 0.0
C     IF(M) 20,20,19
C 19 DO 18 I =1,M
C 18 B1(J,I) = 0.0
C 20 INDEX(J,3) = 0
C 30 DO 550 I=1,N
C
C SEARCH FOR PIVOT ELEMENT
C
C 40 AMAX=0.0
C 45 DO 105 J=1,N
C     IF(INDEX(J,3)=1) 60, 105, 60
C 60 DO 100 K=1,N
C     IF(INDEX(K,3)=1) 80, 100, 715

```

# BEST AVAILABLE COPY

```

80 IF (AMAX-ABS(A(J,K)))>85,100,100
85 IROW=J
90 ICOLUMN=K
A MAX=ABS(A(J,K))
100 CONTINUE
105 CONTINUE
INDEX(ICOLUMN,3)=INDEX(ICOLUMN,3)+1
260 INDEX(I,1)=IPOW
270 INDEX(I,2)=ICOLUMN
C
C INTERCHANGE ROWS TO PUT PIVOT ELEMENT ON DIAGONAL
C
130 IF (IROW-ICOLUMN) 140, 310, 140
140 DETERM=-DETERM
D TERM1=-D TERM1
150 DO 200 L=1,N
SWAP=A(IROW,L)
A1(IROW,L)=A1(ICOLUMN,L)
A1(ICOLUMN,L)=SWAP
160 SWAP=A(IROW,L)
170 A(IROW,L)=A(ICOLUMN,L)
200 A(ICOLUMN,L)=SWAP
IF(M) 310, 310, 210
210 DO 250 L=1, M
SWAP=B(IROW,L)
B1(IROW,L)=B1(ICOLUMN,L)
B1(ICOLUMN,L)=SWAP
220 SWAP=B(IROW,L)
230 B(IROW,L)=B(ICOLUMN,L)
250 B(ICOLUMN,L)=SWAP
C
C DIVIDE PIVOT ROW BY PIVOT ELEMENT
C
310 PIVOT =A(ICOLUMN,ICOLUMN)
PIVOT1 =A1(ICOLUMN,ICOLUMN)
320 CALL FM(P(DETERM,D TERM1,PIVOT ,PIVOT1 ,DETERM,D TERM1)

```

```

330 A(ICOLUMN,ICOLUMN)=1.0
A1(ICOLUMN,ICOLUMN)=0.0
340 DO 350 L=1,N
350 CALL FDY(A(ICOLUMN,L),A1(ICOLUMN,L),PIVOT ,PIVOT1 ,
1 A(ICOLUMN,L),A1(ICOLUMN,L))
355 IF(M) 380, 380, 360
360 DO 370 L=1,M
370 CALL FDY(B(ICOLUMN,L),B1(ICOLUMN,L),PIVOT ,PIVOT1 ,
1 B(ICOLUMN,L),B1(ICOLUMN,L))
1

C REDUCE NON-PIVOT ROWS
C
C 380 DO 550 L1=1,N
390 IF(L1-ICOLUMN) 400, 550, 400
400 T=A(L1,ICOLUMN)
T1 = A1(L1,ICOLUMN)
420 A(L1,ICOLUMN)=0.0
A1(L1,ICOLUMN) = 0.0
430 DO 450 L=1,N
CALL FMP (T,T1,A(ICOLUMN,L),A1(ICOLUMN,L),T4,T5)
450 CALL FSB (A(L1,L),A1(L1,L),T4,T5,A(L1,L),A1(L1,L))
455 IF(M) 550, 550, 460
460 DO 500 L=1,M
CALL FMP (T,T1,B(ICOLUMN,L),B1(ICOLUMN,L),T4,T5)
500 CALL FSB (B(L1,L),B1(L1,L),T4,T5,B(L1,L),B1(L1,L))
550 CONTINUE

C INTERCHANGE COLUMNS
C
C 600 DO 710 I=1,N
610 L=N+1-I
620 IF (INDEX(L+1)-INDEX(L,2)) 630, 710, 630
630 JROW=INDEX(L,1)
640 JCOLUMN=INDEX(L,2)
650 DO 705 K=1,N
SWAP = A1(K,JROW)

```

```
      A1(K,JROW) = A1(K,JCOLUMN)
      A1(K,JCOLUMN) = SWAP
660   SWAP=A(K,JROW)
670   A1(K,JROW)=A(K,JCOLUMN)
700   A1(K,JCOLUMN)=SWAP
705   CONTINUE
710   CONTINUE
      DO 730 K = 1,N
      IF (INDEX(K,3) -1) 715,720,715
715   ID =2
      GO TO 740
      720 CONTINUE
      730 CONTINUE
      ID =1
      740 RETURN
C      LAST CARD OF PROGRAM
END
```

MAT20108  
MAT20109  
MAT20110  
MAT20111  
MAT20112  
MAT20113  
MAT20114  
MAT20115  
MAT20116  
MAT20117  
MAT20118  
MAT20119  
MAT20120  
MAT20121  
MAT20122  
MAT20123  
MAT20124

SIBMAP	DPAF	DECK	PRECISION	FORTRAN	PACKAGE	7090	BE	SYS3
*	DOUBLE							
ENTRY	FAD							
ENTRY	FSB							
ENTRY	FMP							
ENTRY	FDY							
ENTRY	TEST							
FAD	SXA	END+2,2						
	TXI	*+1,4,-2						
	TSX	ALL,2						
	CLA	COMMON+2						
FADE	FAD	COMMON	B1					
	STO	COMMON	A1					
	CLA	COMMON+1	A2					
	STQ	COMMON+1						
	FAD	COMMON+1						
	FAD	COMMON+3	B2					
	FAD	COMMON+1						
	FAD	COMMON						
END	STO*	5,4						
	STQ*	6,4						
	AXT	**,2						
	TRA	7,4						
FSB	SXA	END+2,2						
	TXI	*+1,4,-2						
	TSX	ALL,2						
	CLS	COMMON+3						
	STO	COMMON+3						
	CLS	COMMON+2						
	TXL	FADE,***						
ALL	CLA*	1,4						
	STO	COMMON						
	CLA*	2,4						
	STO	COMMON+1						
	CLA*	3,4						
	STO	COMMON+2						
	CLA*	4,4						

STO COMMON+3  
 TRA 1,2 END+2,2  
 SXA \*+1,4,-2  
 TX1 \*+1,4,-2  
 TSX ALL,2  
 LDQ COMMON  
 FMP COMMON+3  
 STO COMMON+3  
 LDQ COMMON  
 FMP COMMON+2  
 STQ COMMON  
 LDQ COMMON+1  
 STO COMMON+1  
 FMP COMMON+2  
 FAD COMMON+3  
 FAD COMMON  
 FAD COMMON+1  
 TRA END  
 FDY SXA END+2,2  
 TX1 \*+1,4,-2  
 TSX ALL,2  
 CLA COMMON  
 FDP COMMON+2  
 STQ COMMON  
 FAD COMMON+1  
 FDP COMMON+2  
 STQ COMMON+1  
 CLA COMMON+3  
 ANA FDYC  
 FSB COMMON+3  
 FDP COMMON+2  
 FMP COMMON  
 FAD COMMON+1  
 FAD COMMON  
 DCT  
 TRA ERR

DPAF0037  
 DPAF0038  
 DPAF0039  
 DPAF0040  
 DPAF0041  
 DPAF0042  
 DPAF0043  
 DPAF0044  
 DPAF0045  
 DPAF0046  
 DPAF0047  
 DPAF0048  
 DPAF0049  
 DPAF0050  
 DPAF0051  
 DPAF0052  
 DPAF0053  
 DPAF0054  
 DPAF0055  
 DPAF0056  
 DPAF0057  
 DPAF0058  
 DPAF0059  
 DPAF0060  
 DPAF0061  
 DPAF0062  
 DPAF0063  
 DPAF0064  
 DPAF0065  
 DPAF0066  
 DPAF0067  
 DPAF0068  
 DPAF0069  
 DPAF0070  
 DPAF0071  
 DPAF0072

A1 TIMES B2  
 A1 TIMES B1  
 A2 TIMES B1  
 A1 OVER B1  
 REMAINDER A1 OVER B1 + A2  
 DIVIDE BY B1  
 ISOLATE POWER  
 -B2 OVER B1  
 TIMES A1 OVER B1  
 ADD LESSER PARTS  
 ADD A1 OVER B1

```

TRA END
FDYC OCT 377000000000
TEST LDQ TESTC
TXI *+1,4,-2
STQ END
TRA FSB
TESTR LDQ TESTC+1
STQ END
TMI TESTX+2
FSB* 5,4
TMI TESTX+4
PLUS ONE
CLA ERR-1
TESTX LXA END+2,2
TRA 6,4
FAD* 5,4
TMI TESTX+6
ZAC
TRA TESTX
CLS ERR-1
TRA TESTX
DEC 1.
SXA *MWR,4
TSX *MWR,4
MAP
PRINT BUT PROCEED
PZE 1 7/14/64
PZE FORM,5
AXT **,4
TRA END
FORM BCI 5, DBL PREC DIV CKECK
TESTC TRA TESTR
STO* 5,4
COMMON BSS 4
END
DPAF0073
DPAF0074
DPAF0075
DPAF0076
DPAF0077
DPAF0078
DPAF0079
DPAF0080
DPAF0081
DPAF0082
DPAF0083
DPAF0084
DPAF0085
DPAF0086
DPAF0087
DPAF0088
DPAF0089
DPAF0090
DPAF0091
DPAF0092
DPAF0093
DPAF0094
DPAF0095
DPAF0096
DPAF0097
DPAF0098
DPAF0099
DPAF0100
DPAF0101
DPAF0102
DPAF0103
DPAF0104

```

```

$IBFTC GRAPH2 DECK
  SUBROUTINE GRAPH
C   DIMENSION AS IN MGE2
C   DIMENSION DISTL(401),DIA(401),STIFX(401),WTS(401),CONWT(401),
C   1IM(401),JM(401),IBRG(401),IWATR(401),IS(401),DENMAT(7),
C   2DISTT(401),BMTAB(1620),THETA(802),DEF(401),BNFLU(25,25),DIBRG(25)
C   3,IBTAB(25),SFTAB(1620),TITL2(12),NO(400)
C   COMMON AS IN MGE2
C   COMMON N,NO,DISTL,DIA,STIFX,WTS,CONWT,IM,JM,IBRG,
C   2,IBRS,SFTAB,I2,IERROR,TITL2,IXM
C   DIMENSION IPLT(23),GTITLE(21)
C   DATA GTITLE(1)/6H(74H,
C   CALL LGCHAR(8,4HMG2),
C   K=N+1
C   DO 30 I=1,K
C   BMTAB(I)=BMTAB(4*I)/1000.
C   PLT1=450.
C   15=1
C   IGP=9
C   IGS=1
C   IFF=1
C   D01IF=1*23
C   1 IPLT(IF)=0
C   1 COLLECT BEARING POINTS FOR PLOT
C   D022I3=1,IBRS
C   14=IBTAB(I3)
C   BNFLU(I3,1)=DISTL(I4)
C   BNFLU(I3,2)=DEF(I4)
C   BNFLU(I3,3)=BMTAB(I4)
C   22 IF(K-99)5,5,4
C   5 PLT1=AINT((DISTL(K)+99.)/100.*100.
C   IPLT(2)=K
C   IFF=1
C   IGP=(PLT1+99.)*.01
C   IGS=2
C   IF(IGP-35)9,9,19

```

```

19 IGP = (IGP+1)/2
  GO TO 9
  DO 2 IF=1,K
    IF(DISTL(IF)-PLOT1) 2, 2, 3
  3  IPLT(IF+1)=IF-1
    IFF=IFF+1
    PLOT1=PLOT1+450.
  2  CONTINUE
  IPLT(IF+1)=K
C   HAVE NO OF FRAMES SET UP
  PLOT1 = 450.0
C   COMPUTE SCALES FOR DEFL. AND BEND. MOMENT
  9  GDEF=0.
    DO 6 I=1,K
      IF(ABS(DEF(I))-GDEF) 6, 6, 8
      GDEF = ABS(DEF(I)))
    6  CONTINUE
    GBML = 0.
    GBMH = 0.
    DO 12 I=1,K
      IF(BMTAB(I)) 10,12, 11
      10 IF(BMTAB(I)-GBML) 13,12,12
      12 GBML=BMTAB(I)
      13 GBML=8BMTAB(I)
      GO TO 12
      11 IF(BMTAC(I)-GBMH) 12, 12, 14
      14 GBMH = BMTAB(I)
    12 CONTINUE
    GBML=100. * AINT ((GBML -99.)/100.)
    GBMH=100. * AINT ((GBMH +99.)/100.)
    IGBMD=(GBMH-GBML+99.)*.01
    IF(IGBMD-35)24,24,25
    25  IGBMD = (IGBMD+1)/2
    24  IF(IGBMD-10)15,15, 16
    15  IGBMD = IGBMD +IGBMD
    16  GDEF=AINT ((GDEF +.0099)*100.) *.01
    16  GDEF = (GDEF+GDEF+.009)*100.
    16  GRAP073

```

```

17 IF(IGDEF .EQ. 10) 17,17,18
17  IGDEF = ICDEF +IGDEF
18  IF(IGDEF .EQ. 35) 26,26,23
23  IGDEF = (IGDEF+1)/2
26  CONTINUE
      DO 7 1G=1,20
7   GTITLE(IG+1) = TITL2(1G)
      PLOTB=PLOT1
      PLOTA=0.
      DO 20 IC=1,IFF
      1ST = IPLT(IC)
      ISH = IPLT(IC+1)-IST
      CALL FNPLT( GTITLE( 1),32H(28H SECTION DISTANCE IN INCHES,
132H(28H BENDING MOMENT IN KIP FEET,PLOTA,PLOTB, GBML,GBMH,IGP,
2  IGS, IGBMD,2 , 6H(F7.1), 6H(F7.0))
      CALL CURVE (DISTL(1ST), BMTAB(1ST) , ISH, 6H )
      I4=0
      D041 I3=15,IBRS
      IF( IBTAB(13)-IST) 40,40,50
40  I4=I4+1
41  CONTINUE
      I5=IBRS+1
      50  I5=13
      51  IF(14) 52,52,53
      C   GET BEARING VALUES ON DEFL PLOT
      53  CALL CURVE (BNFLU( 1,1),BNFLU( 1,3),I4 ,6H 0)
      52  PLOTA=PLOTB
      20  PLOTB=PLOTB+450.
      I5 = 1
      PLOTA=0.
      DO 21 IC =1,IFF
      1ST = IPLT(IC)
      ISH = IPLT(IC+1)-IST
      CALL FNPLT( GTITLE( 1),32H(28H SECTION DISTANCE IN INCHES,
GRAP0074
GRAP0075
GRAP0076
GRAP0077
GRAP0078
GRAP0079
GRAP0080
GRAP0081
GRAP0082
GRAP0083
GRAP0084
GRAP0085
GRAP0086
GRAP0087
GRAP0088
GRAP0089
GRAP0090
GRAP0091
GRAP0092
GRAP0093
GRAP0094
GRAP0095
GRAP0096
GRAP0097
GRAP0098
GRAP0099
GRAP0100
GRAP0101
GRAP0102
GRAP0103
GRAP0104
GRAP0105
GRAP0106
GRAP0107
GRAP0108
GRAP0109

```

```
126H(22H DEFLECTION IN INCHES , PLOTA,PLOTB,-GDEF,GDEF,IGP,IGS,  
2 1GDEF,2, 6H(F7.1),6H(F6.3)  
CALL CURVE (DISTL(IST), DEF (IST) , ISH , 6H )  
I4=0  
DO 43 I3=15,IBRS  
IF (IBTAB(I3)-IST)44,44,45  
44 I4=I4+1  
43 CONTINUE  
15=IBRS+1  
GO TO 46  
45 I5=13  
46 IF (I4) 54,54,55  
55 CALL CURVE (BNFLU( 1,1), BNFLU( 1,2), 14, .6H O)  
54 PLOTA=PLOTB  
21 PLOTB=PLOTB+450.  
CALL LGCHAR (8, 4H2END)  
RETURN  
END
```

```

LARC VERSION
MATRIX INVERSION WITH ACCOMPANYING SOLUTION OF LINEAR EQUATIONS
INTERNAL DOUBLE PRECISION PIVOT METHOD
NOVEMBER 1992 S GOOD DAVID TAYLOR MODEL BASIN AM MAT2

SUBROUTINE MATINV(A1,N1,B1,M1,DETERM1,ID)

C GENERAL FORM OF DIMENSION STATEMENT
C DIMENSION A(   ,   ),B(   ,   ),INDEX(   ,   ),A1(   ,   ),B1(   ,   )

C EQUIVALENCE (IROW,JROW), (ICOLUMN,JCOLUMN), (AMAX, T, SWAP)
C DIMENSION A(70,70),B(70, 1),INDEX(70,3),A1(70,70),B1(70, 1)
C DOUBLE PRECISION A,B,DETERM,PIVOT,SWAP,T

C INITIALIZATION

C N=N1
C M=M1
C DETERM=0.0
C 10 DO 20 J=1,N
C 11 DO 17 I=1,N
C 17 A(I,J) = A1(I,J)
C 18 IF(M) 20,20,19
C 19 DO 18 I =1,M
C 20 B(J,I) = B1(J,I)
C 20 INDEX(J,3) = 0
C 30 DO 550 I=1,N

C SEARCH FOR PIVOT ELEMENT

C 40 AMAX=0.0
C 45 DO 105 J=1,N
C 46 IF(INDEX(J,3)-1) 60, 105, 60
C 60 DO 100 K=1,N
C 61 IF(INDEX(K,3)-1) 80, 100, 715
C 80 IF (   AMAX -ABSF(A(J,K)) ) 85, 100, 100

```

```

85 IROW=J
90 ICOLUMN=K
95 AMAX = ABSF(A(J,K))
100 CONTINUE
105 CONTINUE
110 INDEX(ICOLUMN,3) = INDEX(ICOLUMN,3) +1
115 INDEX(I,1)=IROW
120 INDEX(I,2)=ICOLUMN
C
C   INTERCHANGE ROWS TO PUT PIVOT ELEMENT ON DIAGONAL
C
130 IF (IROW-ICOLUMN) 140, 310, 140
140 DETERM=-DETERM
150 DO 200 L=1,N
160 SWAP=A(IROW,L)
170 A(IROW,L)=A(ICOLUMN,L)
180 A(ICOLUMN,L)=SWAP
190 IF(M) 310, 310, 210
200 DO 250 L=1, M
210 SWAP=B(IROW,L)
220 B(IROW,L)=B(ICOLUMN,L)
230 B(ICOLUMN,L)=SWAP
240
C
C   DIVIDE PIVOT ROW BY PIVOT ELEMENT
C
250 PIVOT =A(ICOLUMN,ICOLUMN)
260 DETERM=DETERM*PIVOT
270 A(ICOLUMN,ICOLUMN)=1.0
280 DO 350 L=1,N
290 A(ICOLUMN,L)=A(ICOLUMN,L)/PIVOT
300 IF(M) 380, 380, 360
310 DO 370 L=1,M
320 B(ICOLUMN,L)=B(ICOLUMN,L)/PIVOT
330
C
C   REDUCE NON-PIVOT ROWS
C
340
350
360
370

```

```

380 DO 550 L1=1,N
390 IF(L1-1)COLUMN) 400, 550, 400
400 T=A(L1,1)COLUMN)
420 A(L1,1)COLUMN)=0.0
430 DO 450 L=1,N
450 A(L1,L)=A(L1,L)-A(1COLUMN,L)*T
455 IF(M) 550, 550, 460
460 DO 500 L=1,M
500 B(L1,L)=B(L1,L)-B(1COLUMN,L)*T
550 CONTINUE

C
C INTERCHANGE COLUMNS
C
600 DO 710 I=1,N
610 L=N+1-I
620 IF (INDEX(L,1)-INDEX(L,2)) 630, 710, 630
630 JROW=INDEX(L,1)
640 JCOLUMN=INDEX(L,2)
650 DO 705 K=1,N
660 SWAP=A(K,JROW)
670 A(K,JROW)=A(K,JCOLUMN)
700 A(K,JCOLUMN)=SWAP
705 CONTINUE
710 CONTINUE
DO 730 K = 1,N
IF (INDEX(K,3) -1) 715,720,715
715 ID =2
    GO TO 810
720 CONTINUE
730 CONTINUE
ID =1
740 DO 800 J=1,N
    DO 801 I =1,N
801 A(I,J) = A(I,J)
    IF(M) 800,800,802
802 DO 803 I =1,M

```

803 B1(J,I) = B(J,I)  
800 CONTINUE  
800 DTERM1 = DTERM  
810 RETURN  
C LAST CARD OF PROGRAM  
END

MAT2L109  
MAT2L110  
MAT2L111  
MAT2L112  
MAT2L113

MGE2 - SAMPLE INPUT FORM

COLUMN	1	2	4	5	6	8	0	12	BEARING SHAFT	4/1/64
1	66666667	7								
3	45667890	3								
5										
4										
6										
0										
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28	1968•5	34•0	TMGE
29	2028•5	19•5625	TMGE
30	2082•5	21•8125	TMGE
31	2121•5	21•8125	TMGE
32	2160•5	21•375	TMGE
33	2371•0	21•8125	TMGE
34	2443•0	21•8125	TMGE
35	2515•0	19•5625	TMGE
36	2543•5	19•5625	TMGE
37	2559•5	16•0	TMGE
38	2571•5		TMGE
3	3 -0.28355	30000000.	TMGE
	07		TMGE

**Note:** Material 3 as used is identical to Material 1 to illustrate the insertion of new material cards.

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MGE2 - SAMPLE OUTPUT SHEETS

\*\*\* SHAVING SYSTEM PROGRAM MGE2 \*\*\*

SAMPLE CASE 12 BEARING SHAFT 1/1/63

STATION NO.	SECTION DISTANCE (INCH)	FIRST DIAMETER (INCH)	SECOND DIAMETER (INCH)	THIRD DIAMETER (INCH)	CONCENTRATED WEIGHT (LB.)	INPUT DATA		BEARING POSITION	IN WATER	WITH SAND
						A	B			
1	0.	8.0000	-0.	-0.	-0.	-0.	-0.	1	0.	0.
2	2.0000	8.0000	-0.	-0.	-0.	-0.	-0.	1	0.	0.
3	4.0000	18.0000	-0.	-0.	-0.	-0.	-0.	1	0.	0.
4	12.5000	18.0000	-0.	-0.	-0.	-0.	-0.	1	0.	0.
5	24.0000	36.0000	-0.	-0.	-0.	-0.	-0.	1	0.	0.
6	46.5000	36.0000	-0.	-0.	-0.	-0.	-0.	1	0.	0.
7	57.2500	16.0000	-0.	-0.	-0.	-0.	-0.	1	0.	0.
8	68.5000	16.0000	-0.	-0.	-0.	-0.	-0.	1	0.	0.
9	93.5000	33.0000	-0.	-0.	-0.	-0.	-0.	1	0.	0.
10	98.5000	18.0000	-0.	-0.	-0.	-0.	-0.	1	0.	0.
11	109.5000	17.5000	-0.	-0.	-0.	-0.	-0.	1	0.	0.
12	122.7500	31.0000	-0.	-0.	-0.	-0.	-0.	1	0.	0.
13	130.2500	17.0000	-0.	-0.	-0.	-0.	-0.	1	0.	0.
14	316.5000	17.0000	-0.	-0.	-0.	-0.	-0.	1	0.	0.
15	540.5000	17.0000	-0.	-0.	-0.	-0.	-0.	1	0.	0.
16	590.7500	31.0000	-0.	-0.	-0.	-0.	-0.	1	0.	0.
17	598.2500	17.0000	-0.	-0.	-0.	-0.	-0.	1	0.	0.
18	774.5000	17.0000	-0.	-0.	-0.	-0.	-0.	1	0.	0.
19	1008.5000	17.0000	-0.	-0.	-0.	-0.	-0.	1	0.	0.
20	1058.7500	31.0000	-0.	-0.	-0.	-0.	-0.	1	0.	0.
21	1066.2500	17.0000	-0.	-0.	-0.	-0.	-0.	1	0.	0.
22	1242.5000	17.0000	-0.	-0.	-0.	-0.	-0.	1	0.	0.
23	1476.5000	17.0000	-0.	-0.	-0.	-0.	-0.	1	0.	0.
24	1528.7500	31.0000	-0.	-0.	-0.	-0.	-0.	1	0.	0.
25	1534.2500	17.0000	-0.	-0.	-0.	-0.	-0.	1	0.	0.
26	1698.5000	17.0000	-0.	-0.	-0.	-0.	-0.	1	0.	0.
27	1914.5000	17.0000	-0.	-0.	-0.	-0.	-0.	1	0.	0.
28	1968.5000	34.0000	-0.	-0.	-0.	-0.	-0.	1	0.	0.
29	2028.5000	19.5000	-0.	-0.	-0.	-0.	-0.	1	0.	0.
30	2082.5000	21.0000	-0.	-0.	-0.	-0.	-0.	1	0.	0.
31	2121.5000	21.0000	-0.	-0.	-0.	-0.	-0.	1	0.	0.
32	2160.5000	21.0000	-0.	-0.	-0.	-0.	-0.	1	0.	0.
33	2371.0000	21.0000	-0.	-0.	-0.	-0.	-0.	1	0.	0.
34	2443.0000	21.0000	-0.	-0.	-0.	-0.	-0.	1	0.	0.
35	2515.0000	19.5000	-0.	-0.	-0.	-0.	-0.	1	0.	0.
36	2543.5000	19.5000	-0.	-0.	-0.	-0.	-0.	1	0.	0.
37	2559.5000	16.0000	-0.	-0.	-0.	-0.	-0.	1	0.	0.
38	2571.5000	-0.	-0.	-0.	-0.	-0.	-0.	1	0.	0.

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SAMPLE CASE	12 BEARING SHAFT	1	1/1/63
UNDERFLOW AT 13633 IN MO			
UNDERFLOW AT 13624 IN MO			
UNDERFLOW AT 13633 IN MO			
UNDERFLOW AT 13634 IN MO			
UNDERFLOW AT 13635 IN MO			
DEFLECTION AND SLOPE	INFLUENCE NUMBERS ON STATION 1 (FOR CNE INCH OF RISE OF BEARING)		
BRG. NO.	DEFLECTION	SLCPE	
1	1.2301325	-0.01841060	
2	-0.2321747	0.01857397	
3	0.0025792	-0.00020633	
4	-0.0006828	0.00005462	
5	0.0001842	-0.00001474	
6	-0.0000489	0.00000390	
7	0.0000132	-0.0000105	
8	-0.0000036	0.0000028	
9	0.0000010	-0.0000008	
10	-0.0000003	0.0000002	
11	0.0000001	-0.0000000C	
12	-0.0000000	0.0000000	

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SAMPLE CASE 12 BEARING SHAFT 1/1/03

BEARING	REACTION	INFLUENCE	NUMBERS	1.0.	PER	0.001	IN CM	RISE	OF	BEARING
---------	----------	-----------	---------	------	-----	-------	-------	------	----	---------

BRG. NO.	1	2	3	4	5	6	7	8	9	10	11
1	622.0	-805.6	231.9	-61.4	16.6	-4.4	1.2	-0.3	0.1	-0.0	0.0
2	-605.6	1056.3	-334.5	104.0	-26.1	7.4	-2.0	0.5	-0.2	0.0	-0.0
3	231.9	-334.5	130.7	-114.9	46.5	-12.3	3.3	-0.9	0.3	-0.1	0.0
4	-61.4	104.0	-114.9	142.7	-106.7	43.5	-11.6	3.2	-0.9	0.3	-0.1
5	16.6	-26.1	46.5	-104.7	130.5	-106.4	43.8	-11.9	3.5	-1.0	0.2
6	-4.4	7.4	-12.3	43.5	-106.4	140.1	-104.3	44.4	-12.9	3.7	-0.9
7	1.2	-2.0	3.3	-11.6	43.8	-106.3	140.5	-108.3	48.3	-13.0	3.4
8	-0.3	0.5	-0.9	3.2	-11.9	46.4	-108.3	152.7	-121.8	54.7	-13.6
9	0.1	-0.2	0.3	-0.9	3.5	-12.9	48.3	-121.8	176.7	-141.8	53.6
10	-0.0	0.0	-0.1	0.3	-1.0	3.7	-13.8	58.7	-141.8	210.5	-143.1
11	0.0	0.0	-0.1	0.2	-0.7	3.4	-13.6	53.6	-143.1	142.4	-42.0
12	-0.0	0.0	-0.0	0.0	-0.0	0.1	-0.3	1.2	-4.6	30.6	-42.0

	STRAIGHT	LINE	BEARING	REACTIONS (LBS.)
11222.6	33679.8	15265.7	15996.5	15239.3
			15997.3	15276.8
				15845.6
				13438.6
				23299.6
				15898.3

DRG*	12	13	14	15	16	17	18	19	20	21	22
NO.											
1				-0.0							
2				0.0							
3				-0.0							
4				0.0							
5				-0.0							
6				0.1							
7				-0.3							
8				1.2							
9							-4.8				
10							30.6				
11							-42.0				
12							15.2				

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AMPLE CASE 12 BEARING SHAFT 1/1/63

STATION NO.	SHEAR FORCE (KIP. P.)	SHAFTING	SECTION	INTEGRALS	SLOP <sub>L</sub>	(RADIAN)	DEFLECTION (INCH)	BEARING REACTION (LBS.)
1	-0.				-0.0000030	0.00000303	0.00000303	0.
2	-0.02851				-0.0000030	0.00000302	0.00000302	0.
3	-0.05701				-0.0000031	0.00000262	0.00000262	0.
4	10.95231				-0.0000031	-0.00000300	-0.00000300	0.
5	9.72253				1.13-375	0.0000010	-0.00000203	0.
6	-16.13968				234.509	0.0000022	0.0000055	0.
7	-22.97404				-109.619	0.0000027	0.00000501	0.
8	9.89397				-372.843	-0.00000148	-0.0000000	0.
9	8.09011				-146.042	-0.00000563	-0.00000567	0.
10	6.87751				-110.623	-0.00000567	-0.0012472	0.
11	6.08381				-39.335	-0.00000620	-0.0019045	0.
12	5.18013				35.286	-0.00000621	-0.0027341	0.
13	3.57502				68.120	-0.00000618	-0.0031986	0.
14	7.49728				-301.426	0.0000098	-0.0000000	0.
15	6.43347				-309.116	0.00000122	-0.0000003	0.
16	5.19337				33.469	-0.00000630	-0.0024780	0.
17	3.59426				66.385	-0.00000626	-0.0029496	0.
18	7.44903				-299.772	0.00000686	-0.0000001	0.
19	6.44270				-309.156	-0.00000118	-0.0000024	0.
20	5.19293				33.043	-0.00000626	-0.00024573	0.
21	3.58783				65.971	-0.00000623	-0.0029261	0.
22	7.52315				-301.319	0.0000078	-0.0000056	0.
23	6.30847				-302.955	-0.0000083	-0.00000198	0.
24	5.07437				33.286	-0.00000579	-0.0022493	0.
25	3.446926				65.327	-0.00000576	-0.00000625	0.
26	6.333671				-233.004	-0.0000037	-0.00000171	0.
27	15.73454				-365.669	-0.00000526	-0.00000260	0.
28	12.25909				390.159	-0.00000503	-0.00000576	0.
29	-3.18736				662.311	-0.00000319	-0.00070772	0.
30	-7.18816				382.171	0.0001033	-0.0048337	0.
31	5.03098				30.086	0.0001343	-0.00000358	0.
32	1.35180				154.552	0.0001491	0.0054330	0.
33	-17.64124				-1559.911	-0.0001483	0.0297298	0.
34	35.02704				-3071.604	-0.0007453	-0.00000561	0.
35	28.23470				-737.181	-0.0012424	-0.0752001	0.
36	1.478016				-22.582	-0.0012959	-0.1116143	0.
37	0.59473				-3.583	-0.0012966	-0.1323576	0.
38	-0.00001				-0.015	-0.0012969	-0.1479202	0.

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SAMPLE CASE 12 BEARING SHAFT 1/1/63

STATION NO.	SECTION DISTANCE (INCH)	SHAFTING WEIGHT (LB/IN.)	WEIGHT AND STIFFNESS FACTORS STIFFNESS (1/EI) (X0.000000000001)	CONCENTRATED WEIGHT OR REACTION (LB.)	BEARING POSITION		
					0°	90°	180°
1	0.	-14.25228	165.788400	0.	0.	0.	0.
2	2.00000	-14.25228	165.788400	0.	0.	0.	0.
3	4.00000	-72.15477	6.488727	11288.64	0.	0.	0.
4	12.50000	-72.15477	6.488727	0.	0.	0.	0.
5	24.00000	-288.6187	0.489295	-23100.00	0.	0.	0.
6	40.50000	-288.6187	0.489295	0.	0.	0.	0.
7	57.25000	-72.15477	6.488727	33679.78	0.	0.	0.
8	68.50000	-72.15477	6.488727	0.	0.	0.	0.
9	93.50000	-242.5199	0.572602	0.	0.	0.	0.
10	98.50000	-72.15477	0.488727	0.	0.	0.	0.
11	109.50000	-68.2018	7.246302	0.	0.	0.	0.
12	122.7500	-214.0164	0.752296	0.	0.	0.	0.
13	130.2500	-64.3602	8.136423	0.	0.	0.	0.
14	306.50000	-64.3602	8.136423	15285.74	0.	0.	0.
15	590.5000	-64.3602	8.136423	15998.47	0.	0.	0.
16	590.7500	-214.0164	0.752296	0.	0.	0.	0.
17	598.2500	-64.3602	8.136423	0.	0.	0.	0.
18	774.5000	-64.3602	8.136423	15239.26	0.	0.	0.
19	1008.5000	-64.3602	8.136423	15997.29	0.	0.	0.
20	1058.7500	-214.0164	0.752296	0.	0.	0.	0.
21	1066.2500	-64.3602	8.136423	15998.47	0.	0.	0.
22	1242.5000	-64.3602	8.136423	15278.81	0.	0.	0.
23	1476.5000	-64.3602	8.136423	15885.60	0.	0.	0.
24	1526.7500	-214.0164	0.752296	0.	0.	0.	0.
25	1536.2500	-64.3602	8.136423	0.	0.	0.	0.
26	1698.5000	-64.3602	8.136423	13439.61	0.	0.	0.
27	1914.5000	-64.3602	8.136423	23293.63	0.	0.	0.
28	1968.5000	-257.4409	0.569191	0.	0.	0.	0.
29	2028.5000	-74.0093	4.636726	0.	0.	0.	0.
30	2082.5000	-94.3380	3.542795	0.	0.	0.	0.
31	2121.5000	-94.3380	3.642795	15698.34	0.	0.	0.
32	2160.5000	-90.2282	3.682323	0.	0.	0.	0.
33	2371.0000	-94.3380	3.642795	0.	0.	0.	0.
34	2443.0000	-94.3380	3.642795	59460.61	0.	0.	0.
35	2515.0000	-74.0093	4.636726	0.	0.	0.	0.
36	2543.5000	-74.0093	4.636726	-24343.00	0.	0.	0.
37	2559.5000	-49.5618	10.361650	0.	0.	0.	0.
38	2571.5000	-0.	0.	0.	0.	0.	0.

TOTAL SHAFT WEIGHT (INCLUDING CONCENTRATED LOADS) = -289622.00 LB.  
DISTANCE OF CENTER OF GRAVITY FROM STATION NO. 1 = 1326.7418 INCH

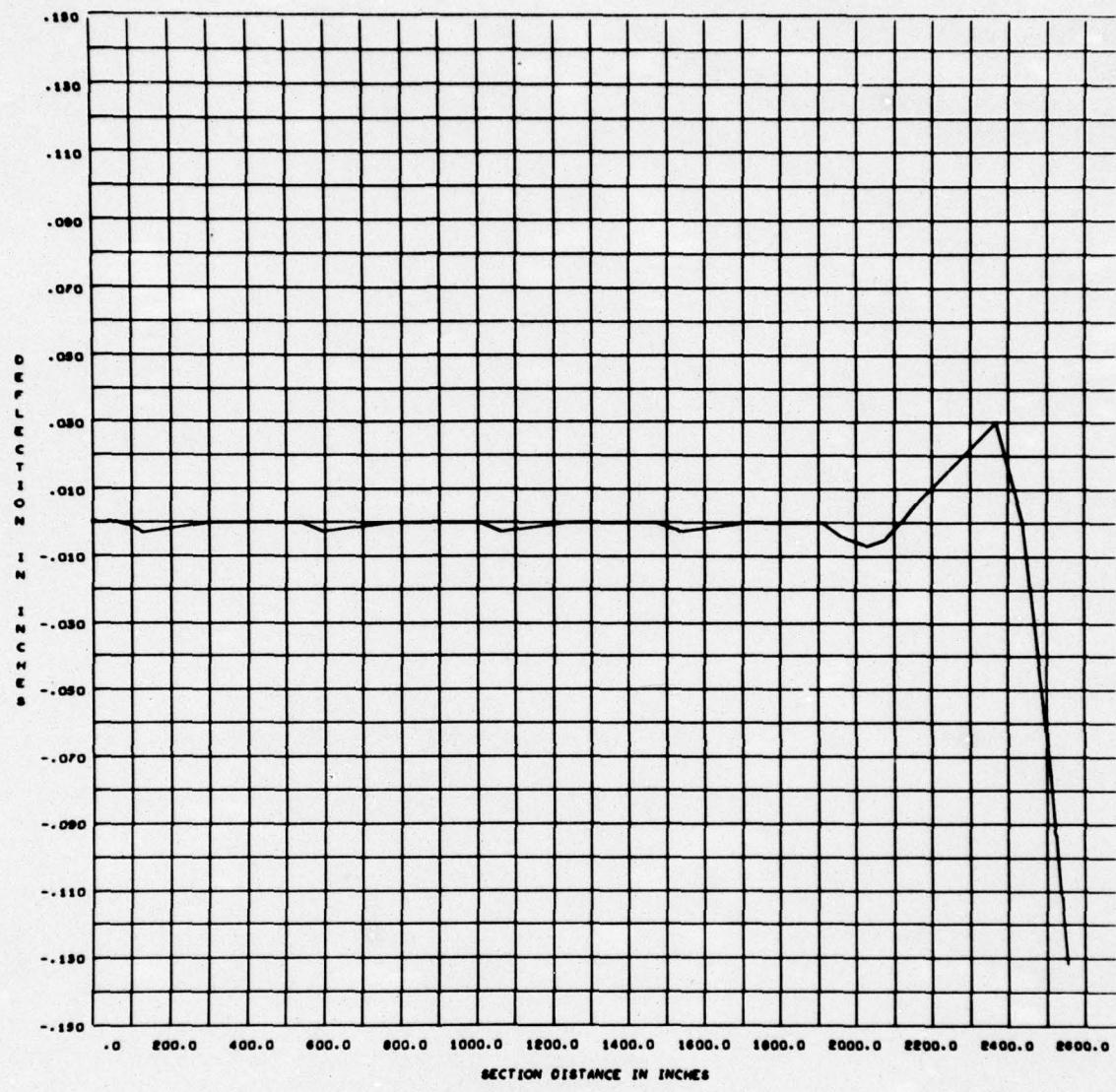
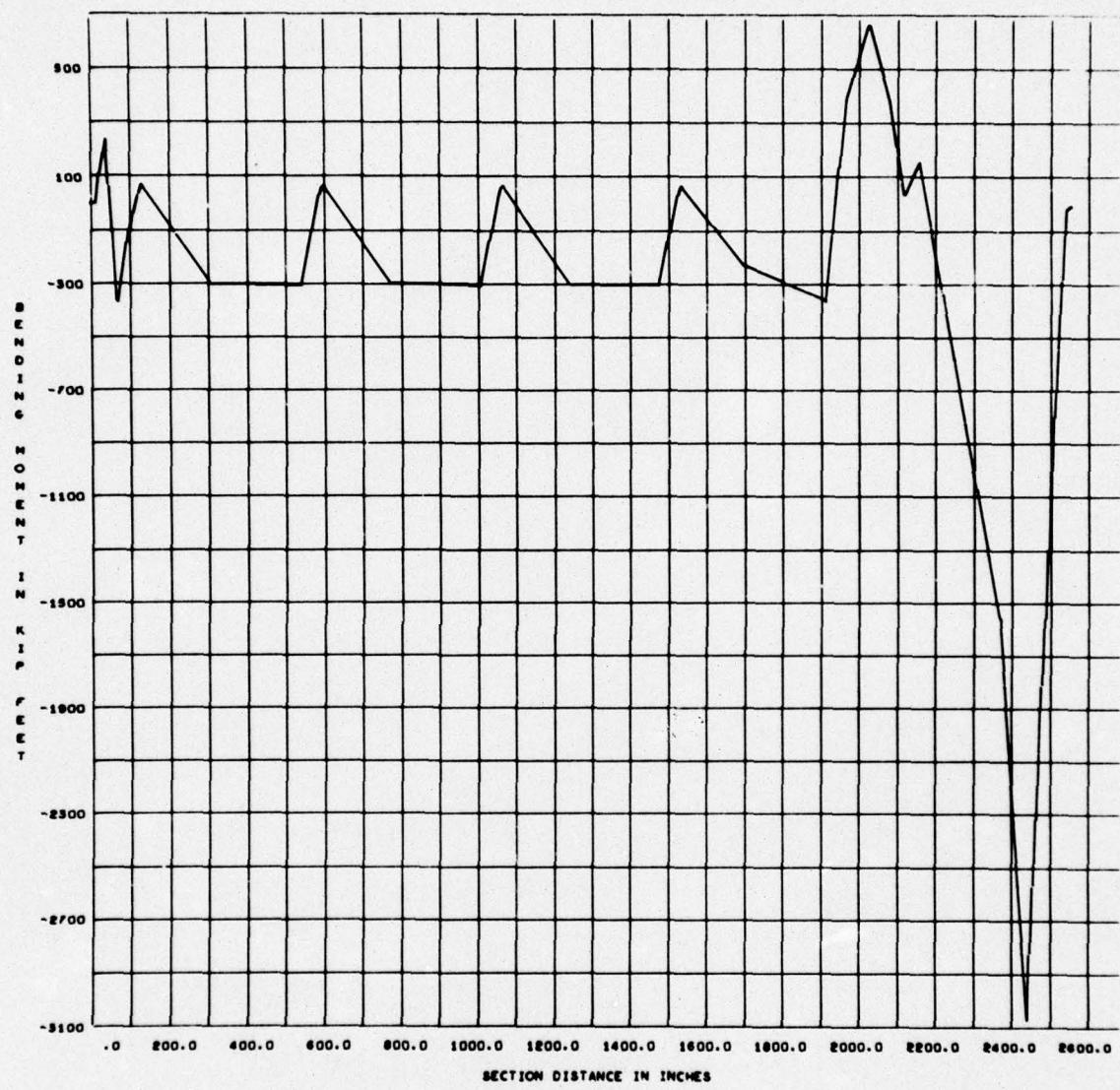


Figure A.1 - Sample Graphic Output



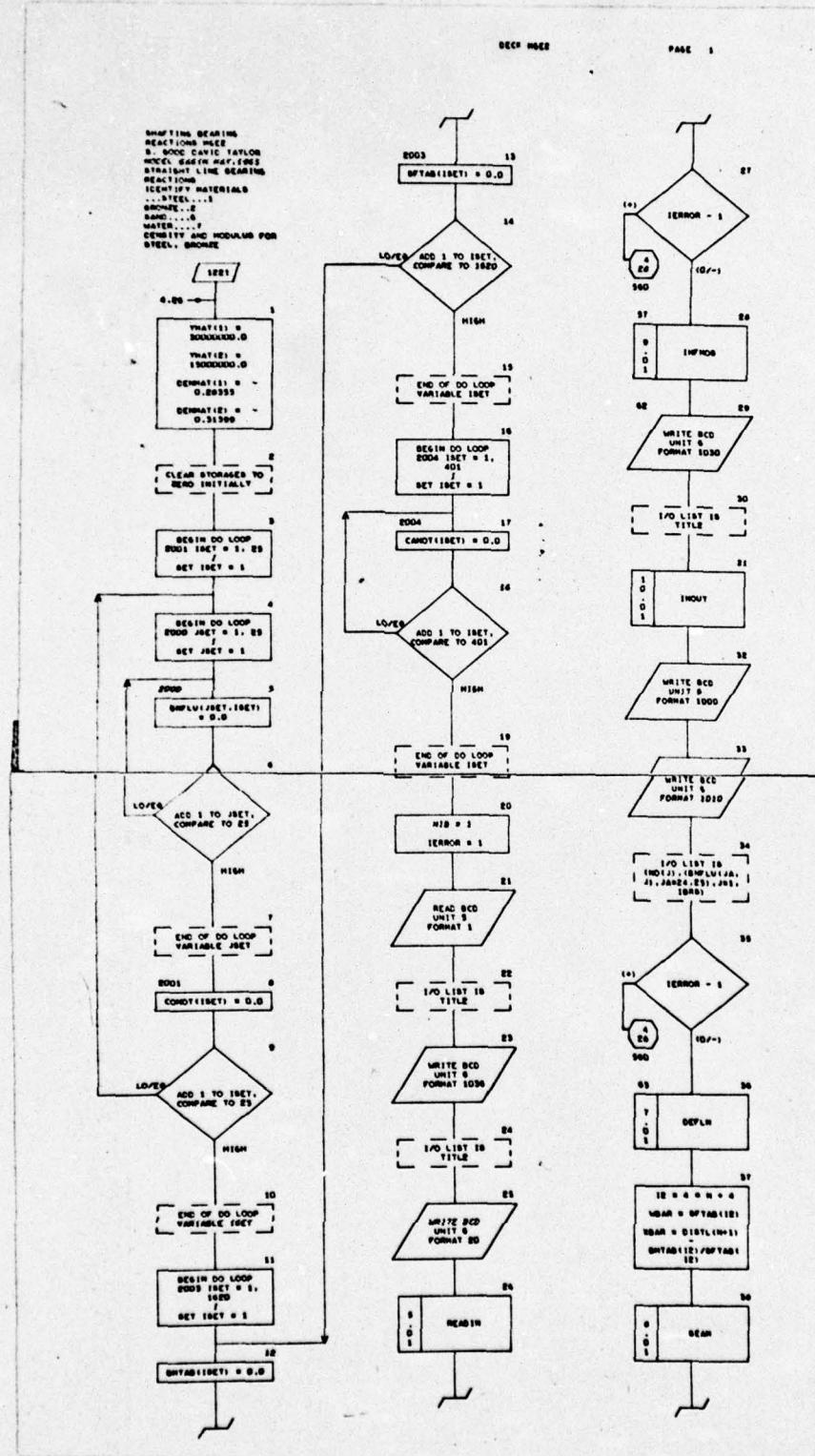
SAMPLE CASE 12 BEARING SHAFT 1/1/83

1

Figure A. 2 - Sample Graphic Output

## FLOW CHART

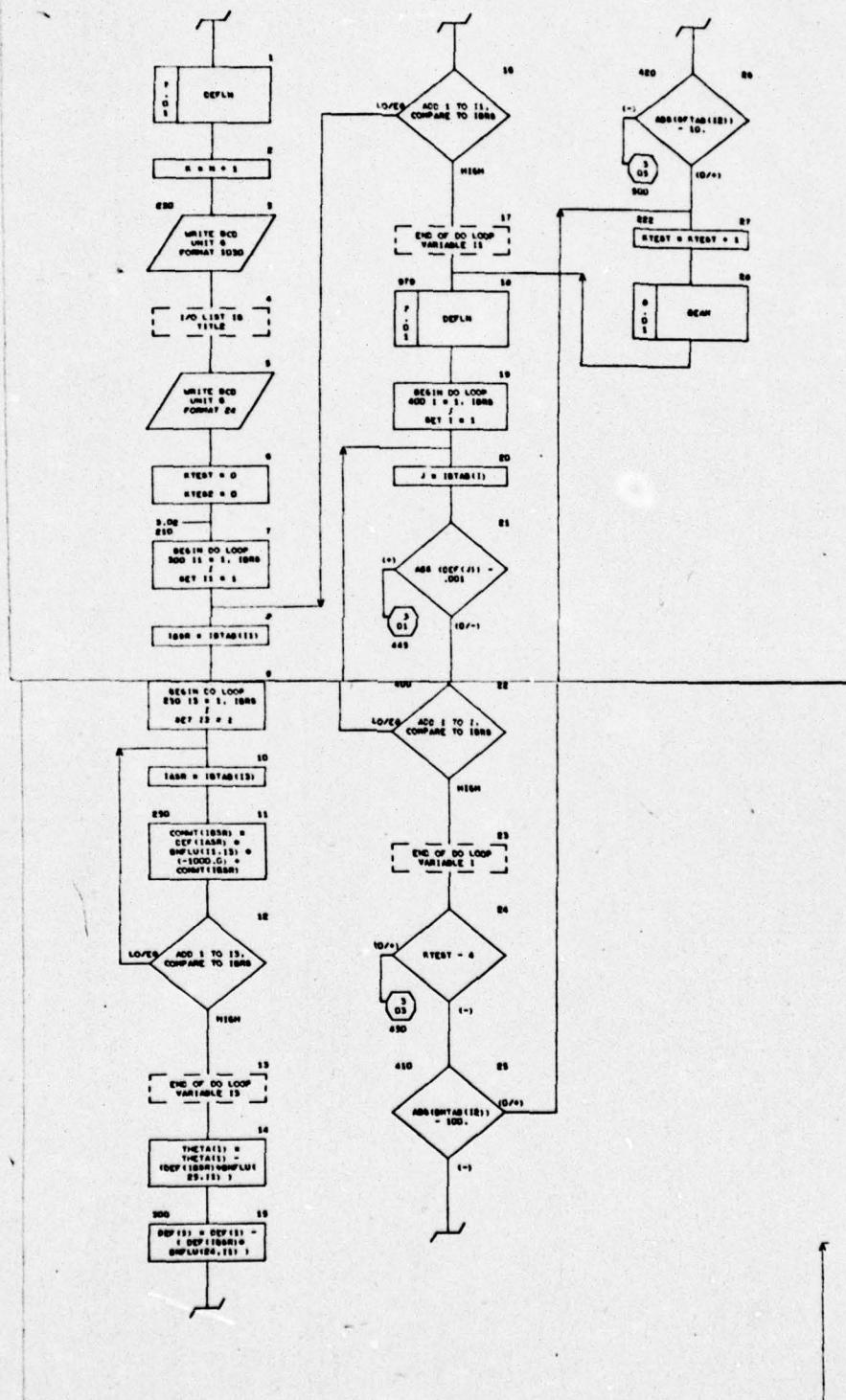
# BEST AVAILABLE COPY



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CECE 1002

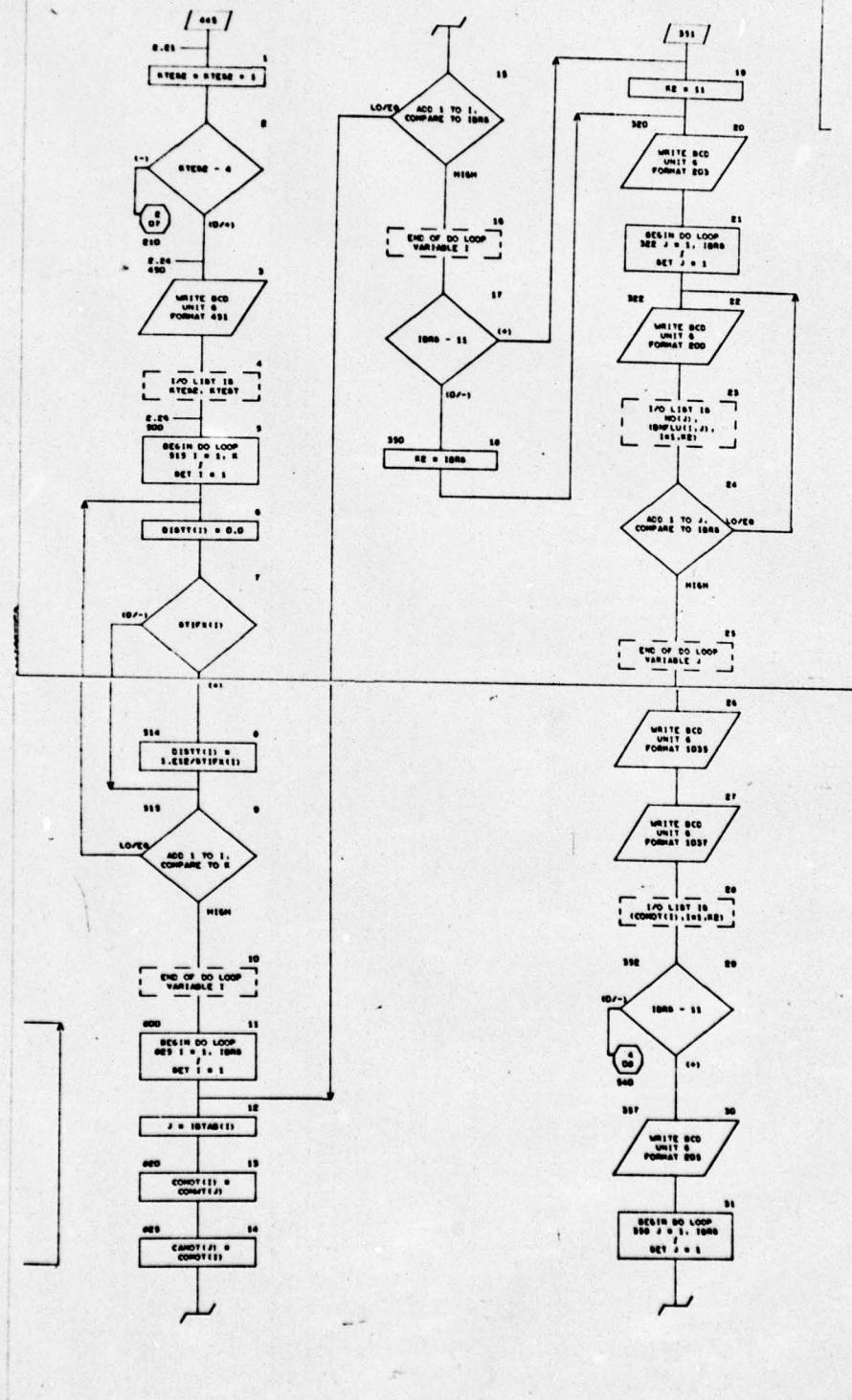
PAGE 8



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DECEMBER

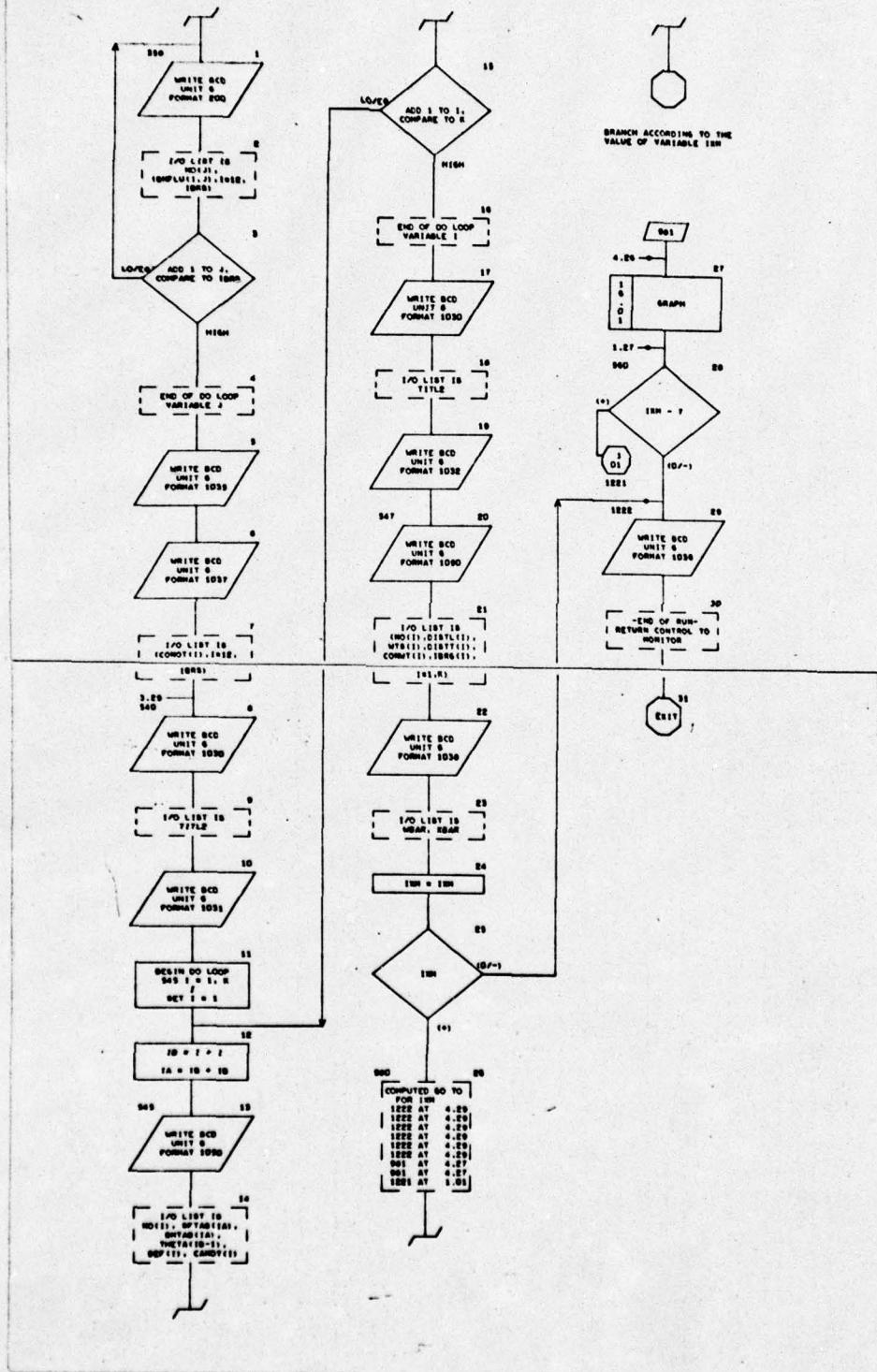
PAGE



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DECK PAGE

PAGE 4

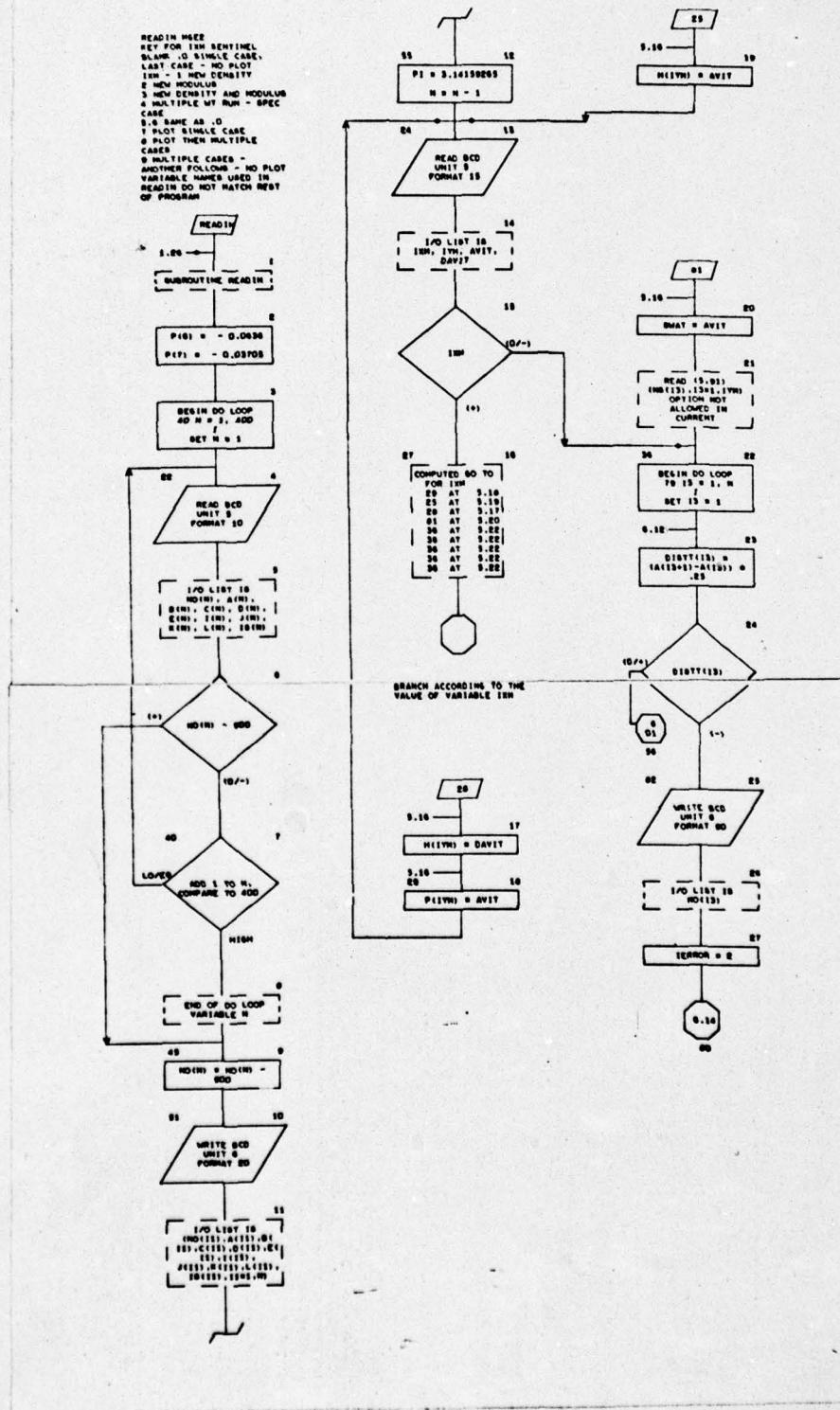


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SWERDLOW TIME READERS

## DECK AGES

PAGE

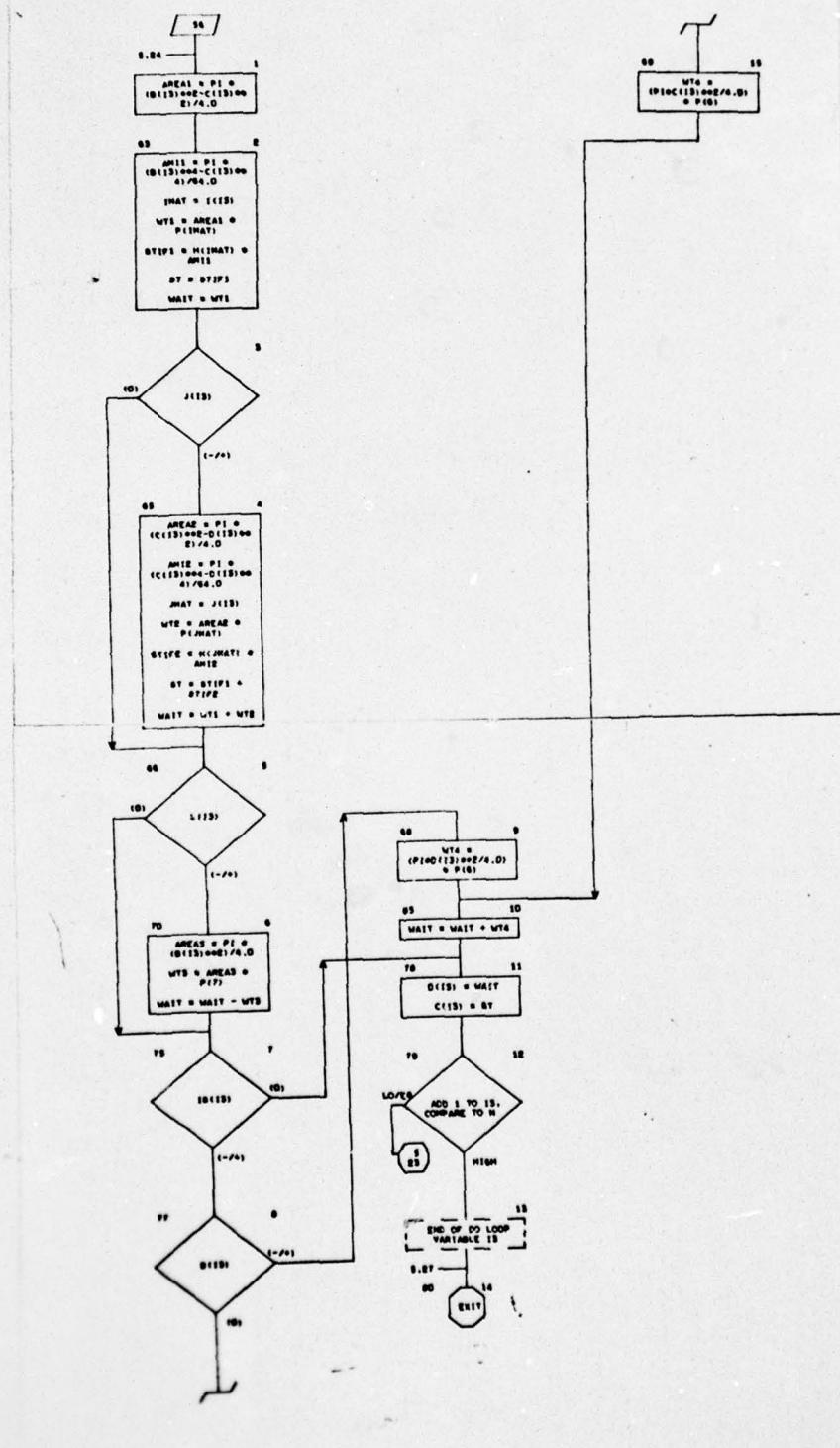


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DECK READ

Page

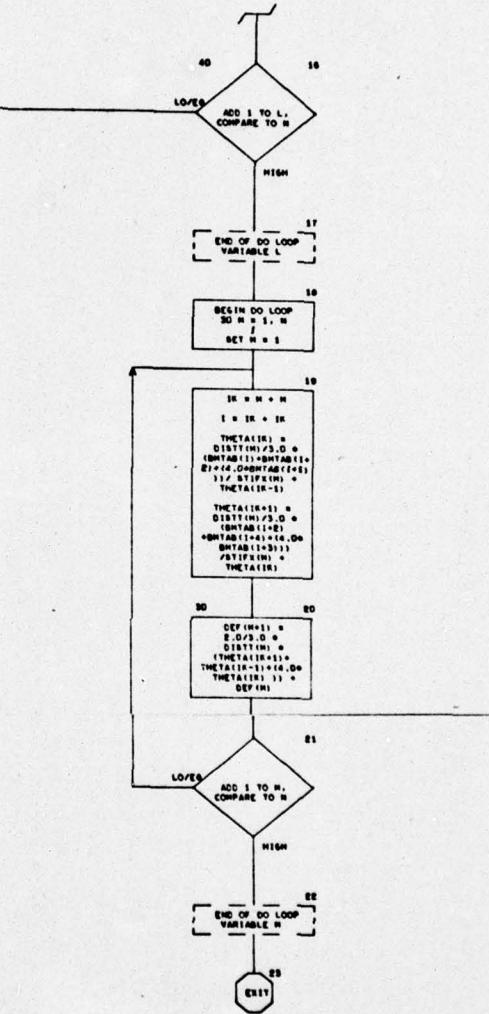
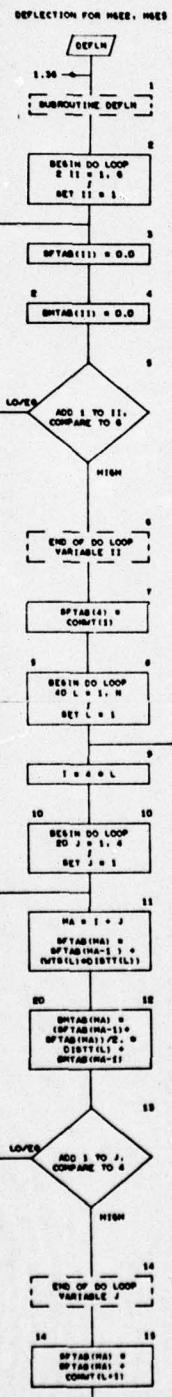
**SUBROUTINE READIN**



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0000 0000

PAGE 1



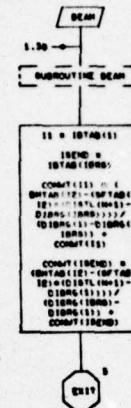
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### DECK BEAMS

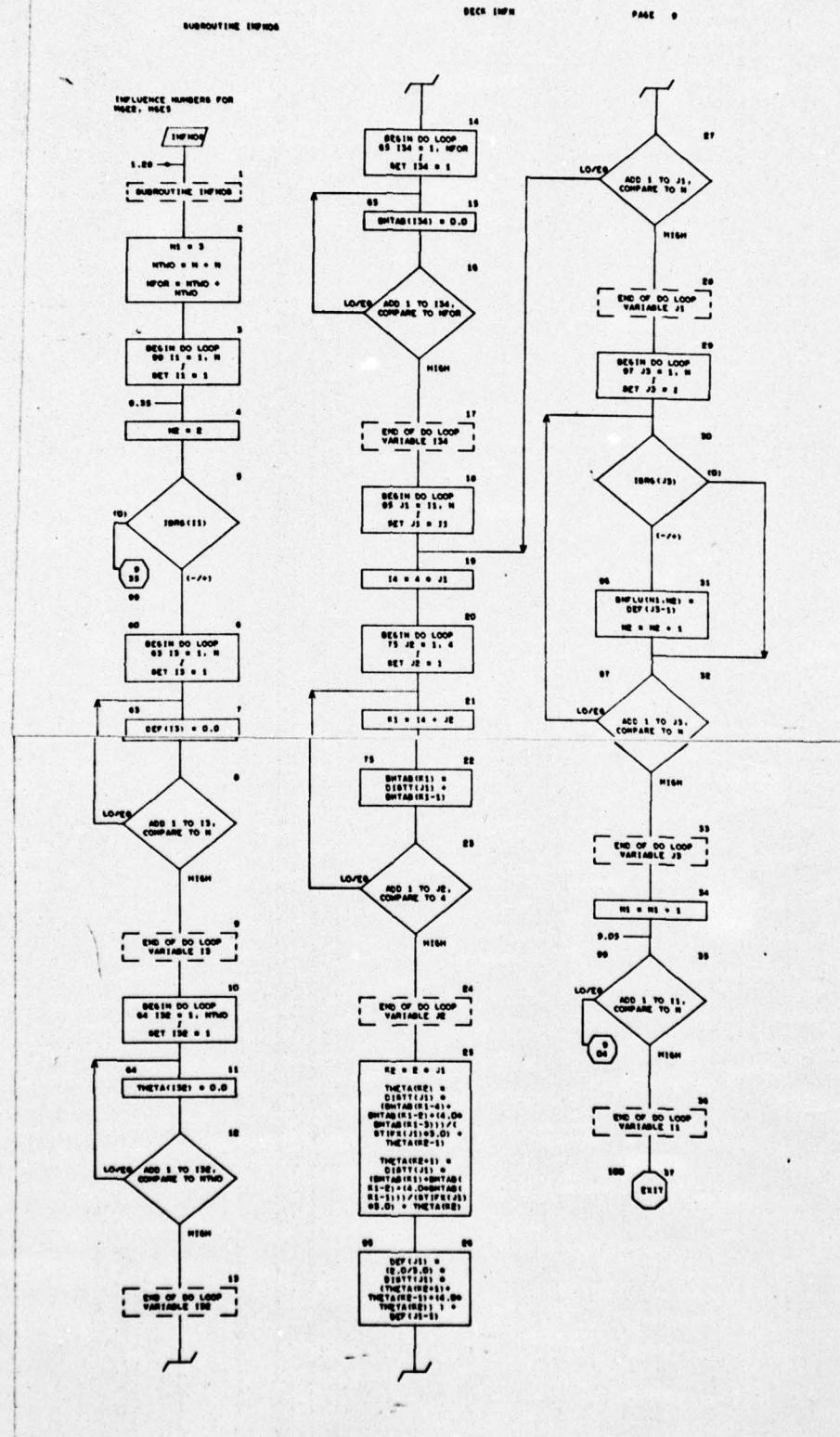
PAGE 8

### OUTABOUT THE GREAT

DEAN SUBROUTINE FOR MICE  
AND MOLES



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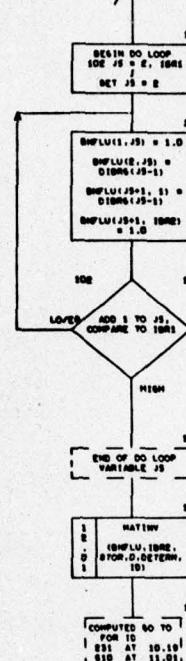
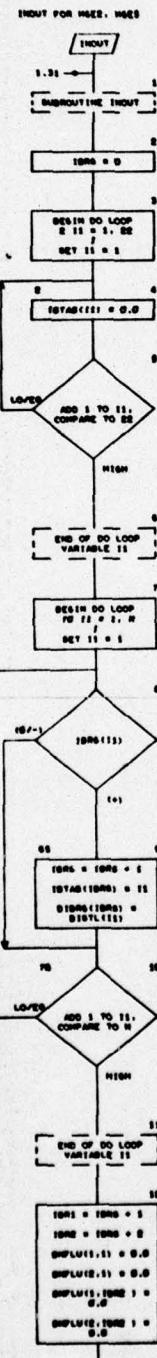


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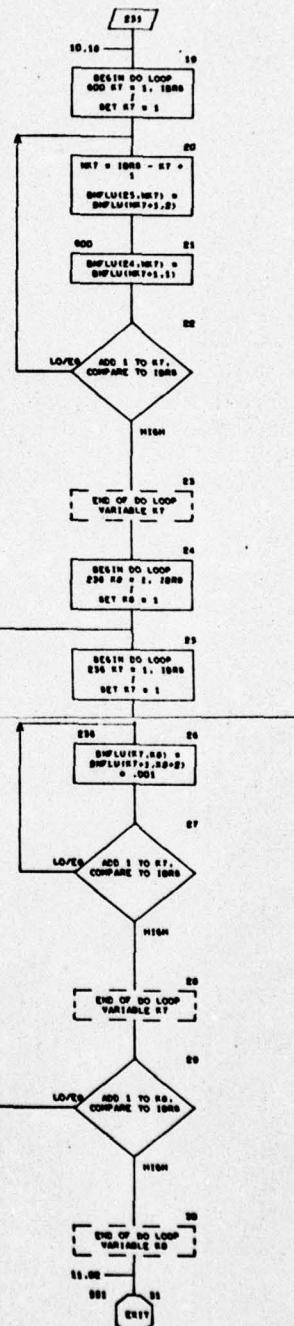
© 1997 DOW TINT. 110001

0000 1000

PAGE 11

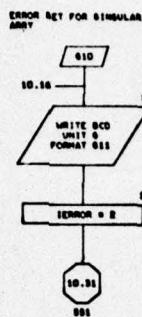


BRANCH ACCORDING TO THE  
VALUE OF VARIABLE ID



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ROUTINE INOUT DECK INOUT PAGE 15



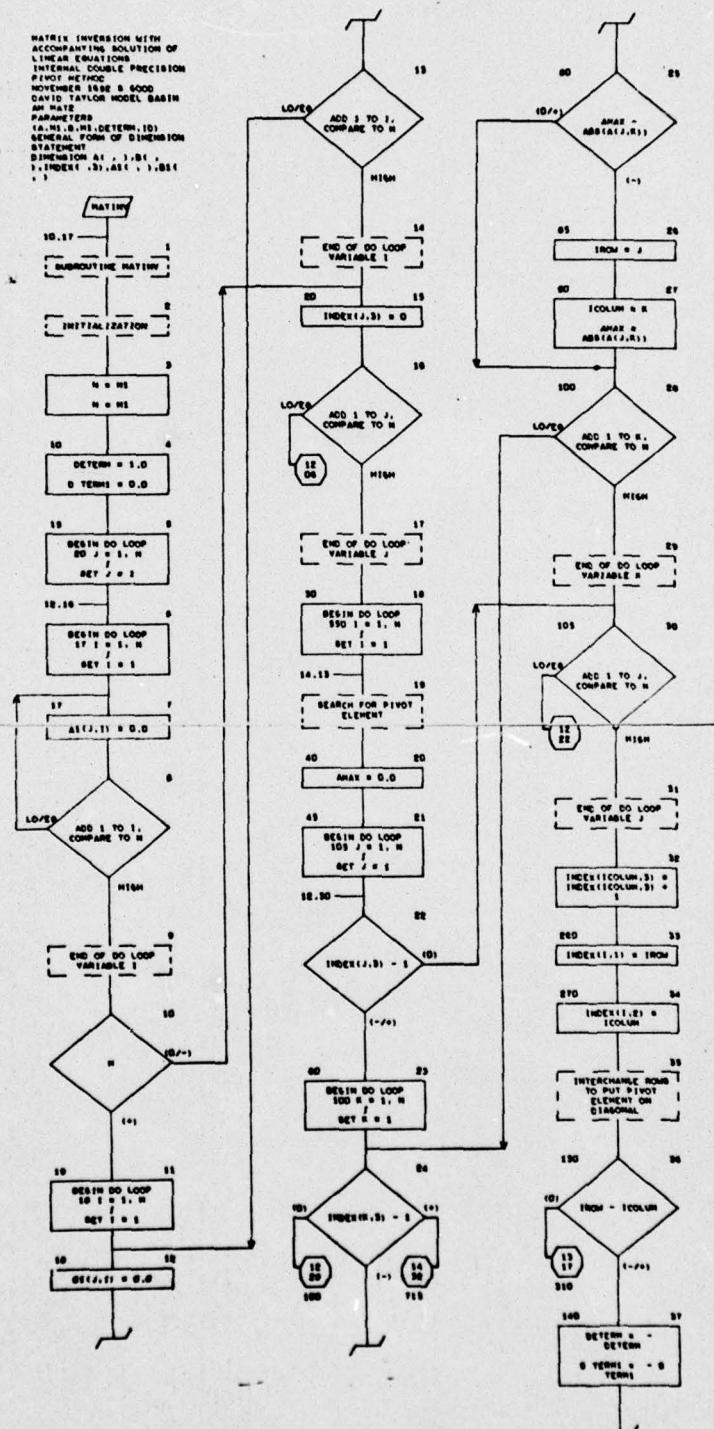
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DECA MATS

PAGE 1

**SUBROUTINE MATINV**

MATRIX INVERSION WITH  
ACCOMPANYING SOLUTION OF  
LINEAR EQUATIONS  
INTERNAL DOUBLE PRECISION  
PIVOT METHOD  
NOVEMBER 1992 8:00D  
DAVID TAYLOR MODEL BABIN  
AM MATE  
PARAMETERS  
(A,M,B,N,DETERM,1D)  
GENERAL FORM OF DIMENSION  
STATEMENT  
DIMENSION A1 : 1,81 :  
1,INDEX1 : 1,81,1 : 1,81

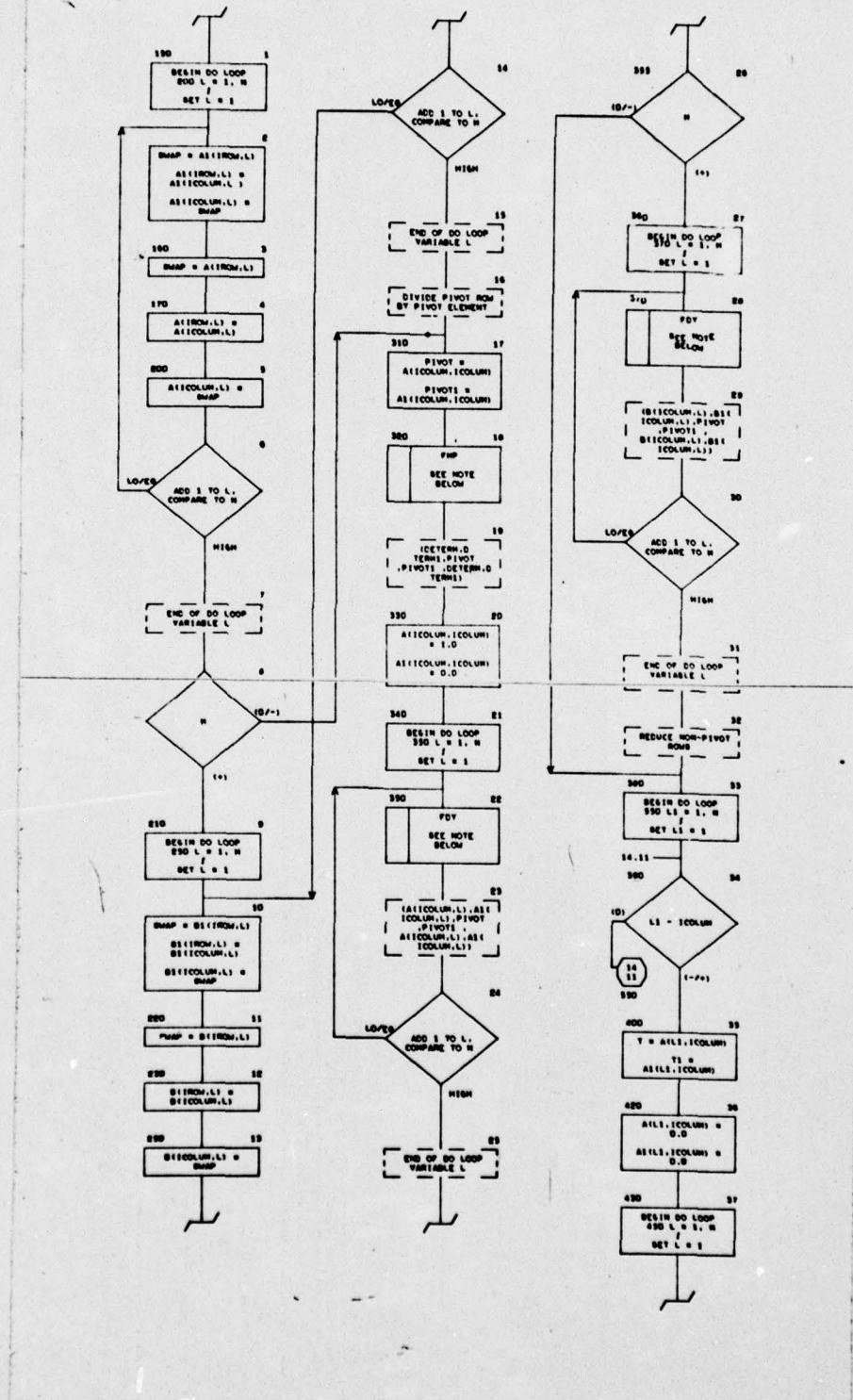


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SUBROUTINE MATRIX

SEE NOTE

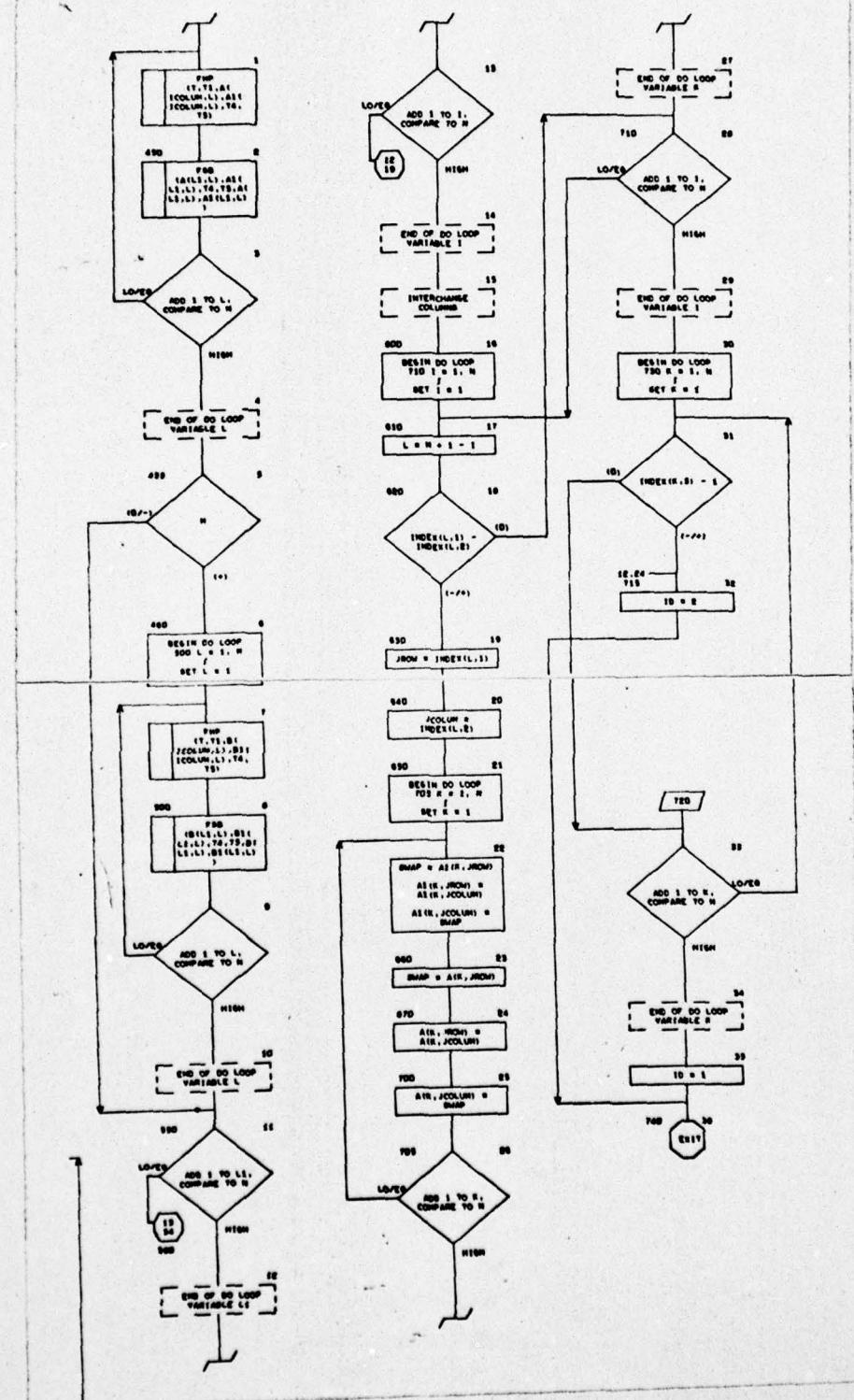
PAGE 13



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**DECK RATE**

PAGE 10



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DECK PAGE

PAGE 10

SUBROUTINE MATRIX

LAST CARD OF PROGRAM

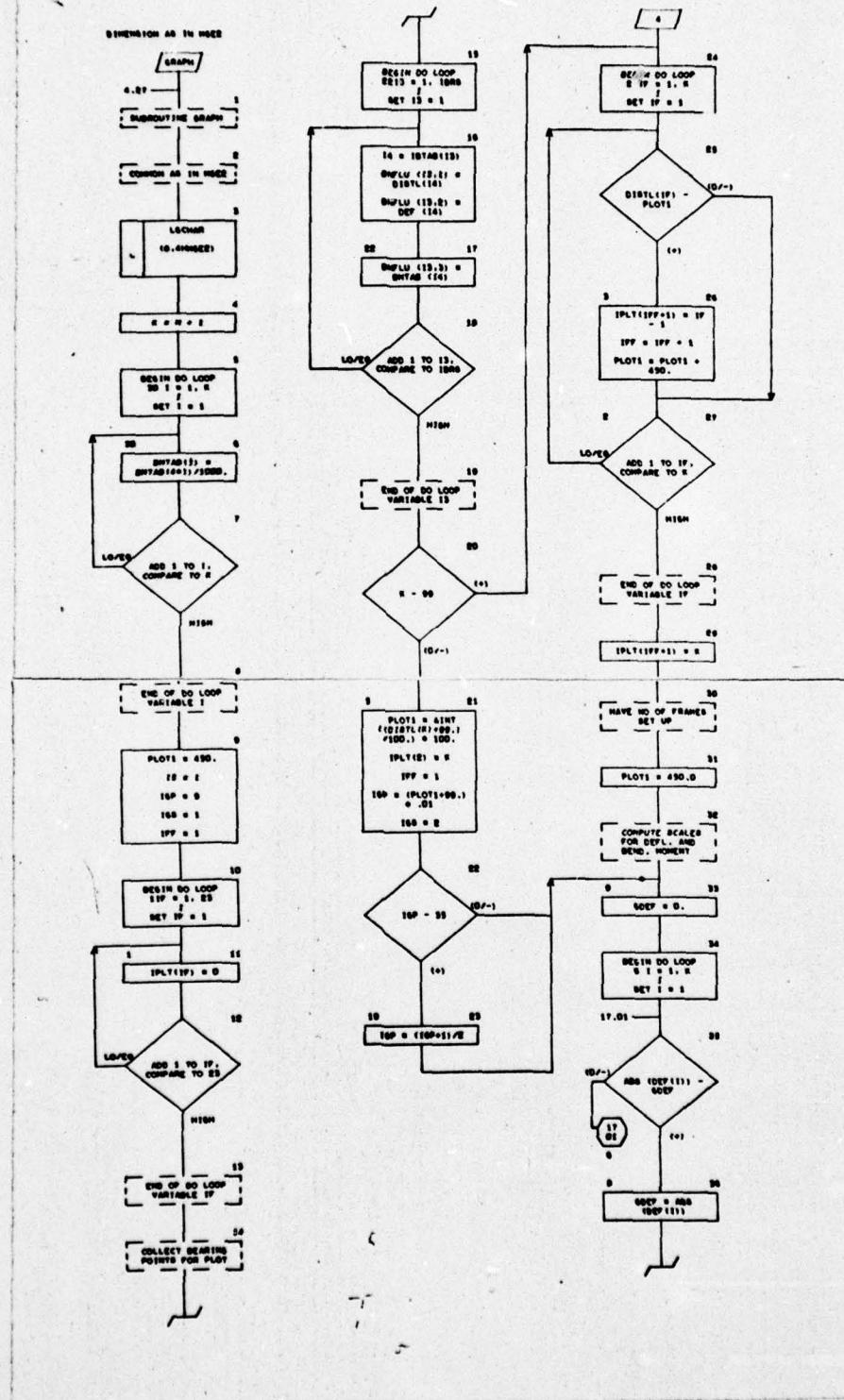


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DATA COMPLIANCE

## DECK GRAPH

PAGE 10

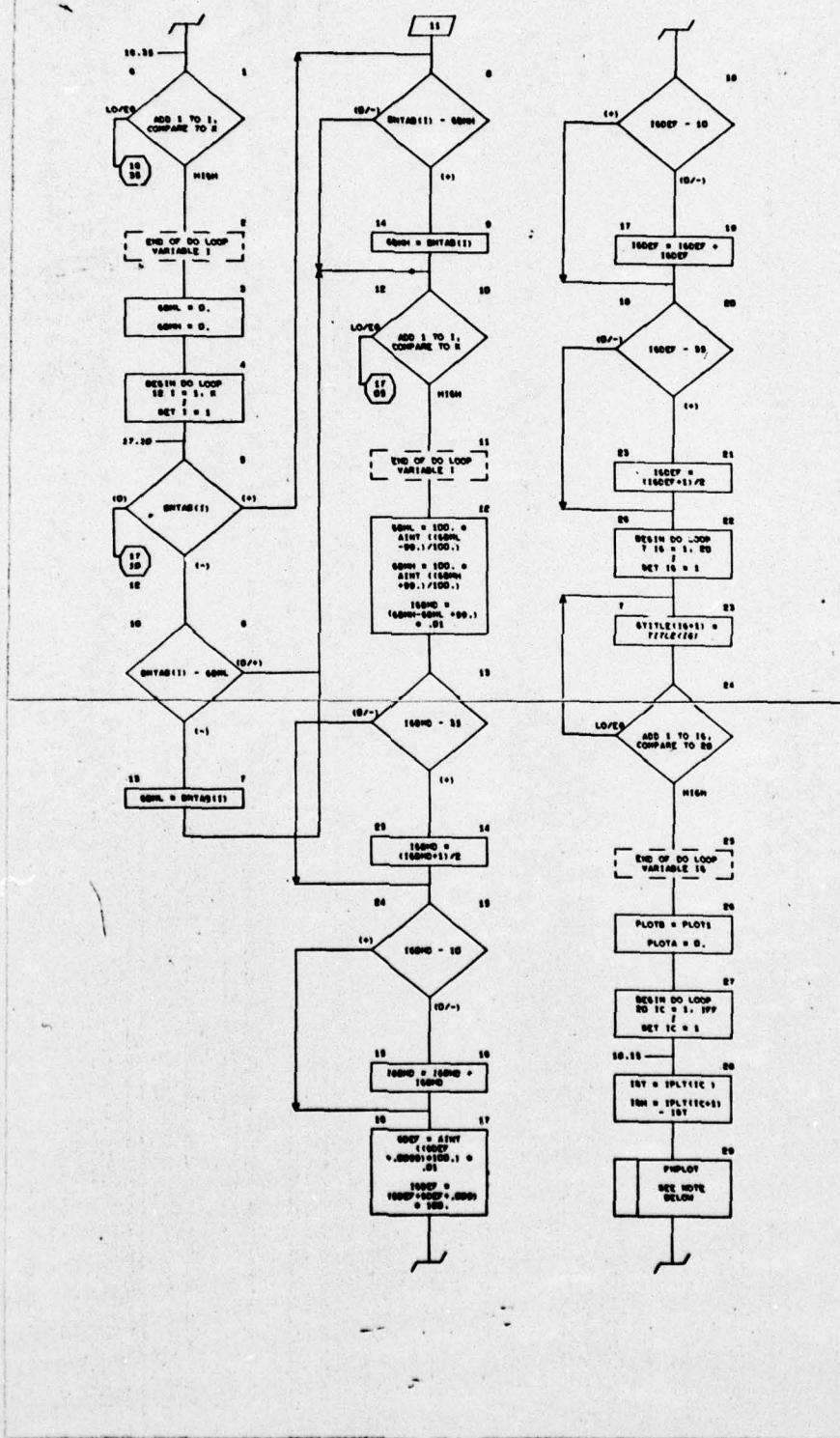


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© 1990 by the American Mathematical Society

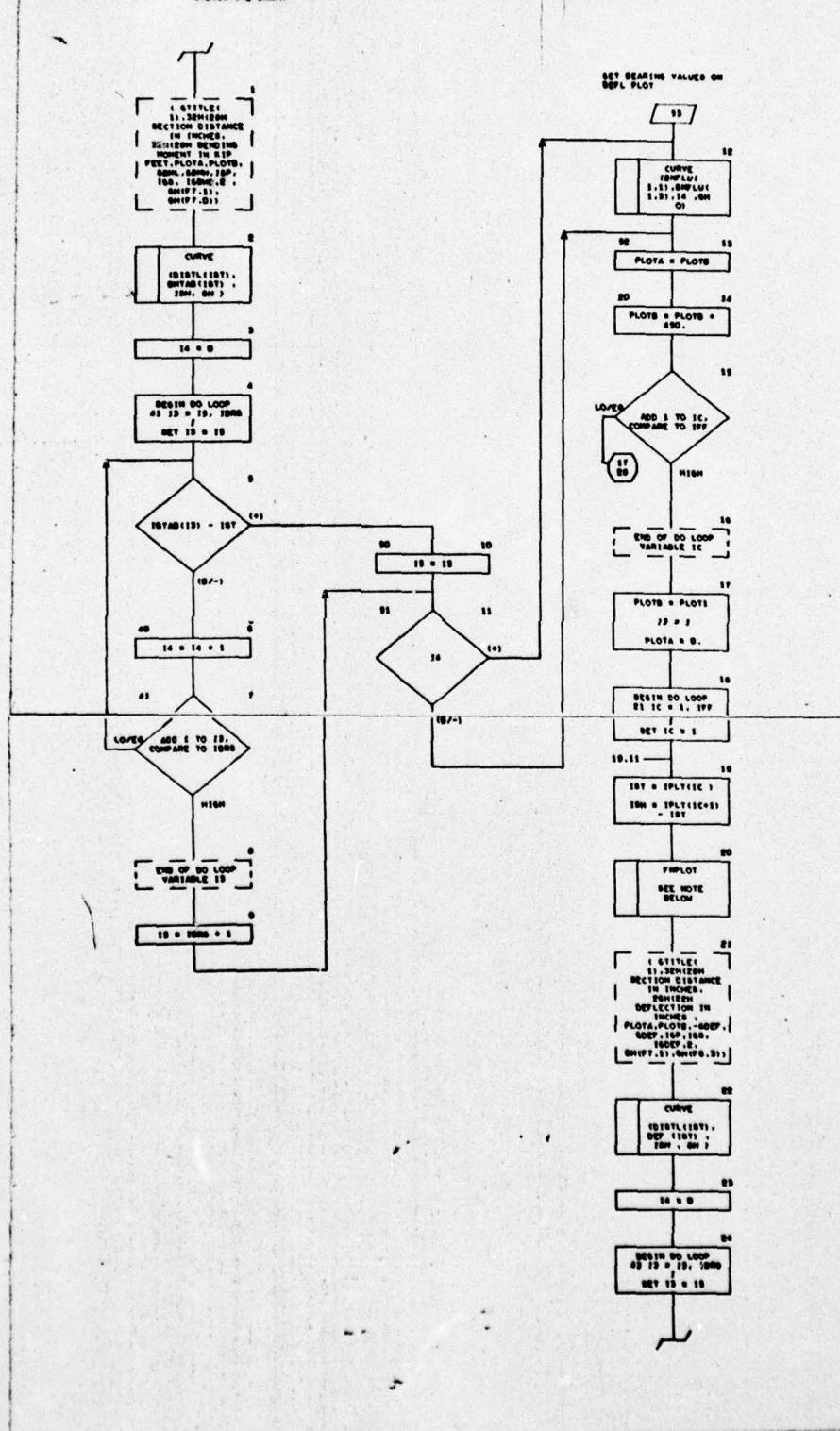
888 GRAPHICS

PAGE 11



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PAGE 10

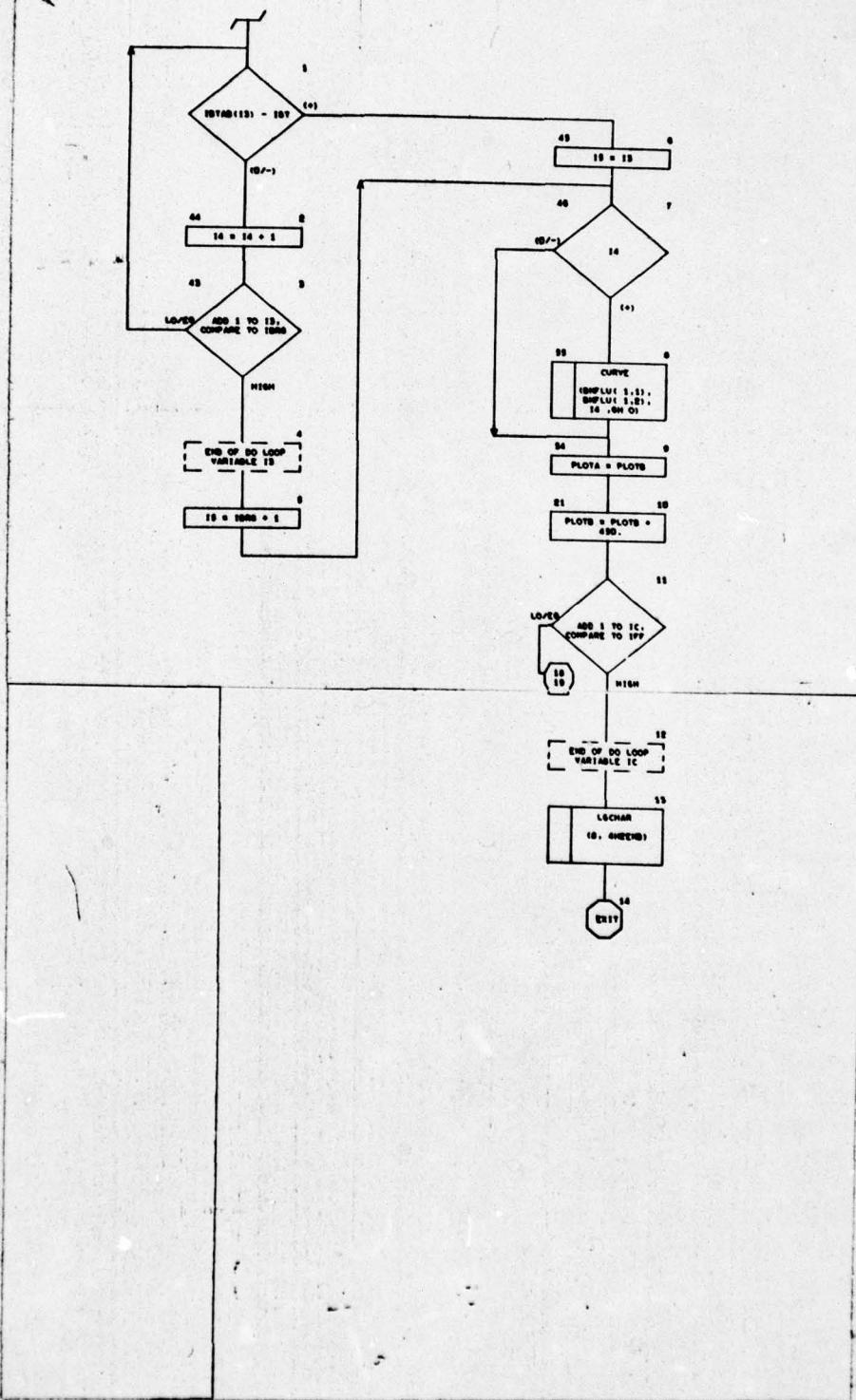


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ROUTINE GRAPH

DECK GRAPH

PAGE 10



AD-A041 797

NAVAL SHIP RESEARCH AND DEVELOPMENT CENTER BETHESDA --ETC F/G 13/10  
SHIP PROPULSION SHAFTING BEARING REACTION PROGRAMS MGE2 AND MGE--ETC(U)

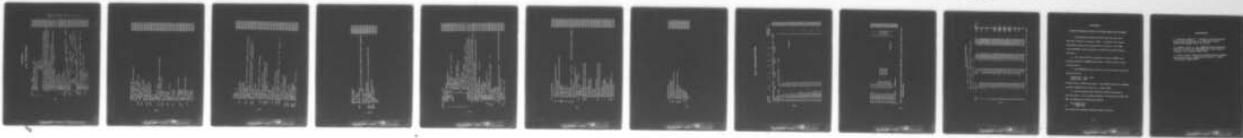
AUG 67 S E GOOD

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AML-70-67

NL

2 OF 2  
ADA  
041797



END  
DATE  
FILMED  
8-77

## APPENDIX B

### MGES - PROGRAM LISTING

```

$IBFTC MGES      DECK
C   SHAFTING BEARING REACTIONS MGES
C   BEARINGS NOT ON STRAIGHT LINE
C   IDENTIFY MATERIALS ***STEEL***1
C   BRONZE***2
C   SAND***6
C   WATER***7
C
C   DIMENSION DISTL(401),DIA(401),STIFX(401),WTS(401),CONWT(401),
C   LIM(401),JM(401),IBRG(401),IWATR(401),IS(401),YMAT(7),DENMAT(7),
C   2D1STT(401),RMTAB(1620),THETA(802),DEF(401),BNFLU(25,25),DIBRG(25)MGE50010
C   3,1BTAB(25),SFTAB(1620),TITL2(12),TITL5(12),XBRG(25),NO(400)
C
C   DIMENSION CANOT(401),CONOT(25)
C   COMMON N,NO,DISTL,DIA,STIFX,WTS,CONWT,IM,JM,IBRG,
C   1,IWATR,IS,YMAT,DENMAT,DISTT,BMTAB,THETA,DEF,BNFLU,DIBRG,IBTAB,
C   2,IBRS,SFTAB,12,ERROR,      TITL2,IM
C
C   DIMENSION NS(50)
C
C   COMMON SWAT,NS,YM
C   COMMON TITL5,XBRG
C
C   1  FORMAT(12A6)
C   2  FORMAT(11,5F11.8)
C
C   1030 FORMAT(1H120X,12A6///)
C   1032 FORMAT(11OH0)      *   WITH CERTAIN BEARINGS LOWERED
C   1R RAISED FROM ORIGINAL STRAIGHT LINE DATUM
C
C   1037 FORMAT(F14.1,10F10.1)
C
C   1040 FORMAT(11OH STATION)      SHEAR FORCE      MOMENT
C   1      SLOPE      DEFLECTION      BEARING /
C   2      113H      NO.      (KIP.)      (KIP. INCH)
C   1      (RADIAN)      (INCH)      REACTION (LBS.)
C
C   1050 FORMAT(19,-3PF21.5,F19.3,0PF20.7,F20.7,F16.1)
C
C   1097 FORMAT(11)
C   1036 FORMAT(1H1 20X 45H ***)
C   1///20X,1?A6/20X12A6)
C
C   DENSITY AND MODULUS FOR STEEL, BRONZE
C   1221 YMAT(1)=30000000.0
C   YMAT(2)=15000000.0
C   DENMAT(1)=-0.28355

```

B. 1

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```

DENMAT(2)=-0.31399
C      CLEAR STORAGE'S TO ZERO INITIALLY
      DO 2001 ISET=1,25
      DO 2000 JSET = 1,25
2000  BNFLU(JSET,ISET) = 0.0
      XBRG(ISET) = 0.0
2001  CONOT(ISET) = 0.0
      DO 2003 ISET=1,1620
      BMTAB(ISET)=0.0
2003  SFTAB(ISET)=0.0
      DO 2004 ISET=1,401
2004  CANOT(ISET)=0.0
      N76 =5
      N77=1
      TERROR = 1
      READ (5,1) TITL5
      READ (5,2) IMOVE, (XBRG(I77),I77=N77,N76)
231   IF (IMOVE) 220,230,220
230   N76 =N76+5
      N77=N77+5
      GO TO 231
220   CONTINUE
      READ (5,1) TITL2
      NIB=1
      50   CALL READIN
            IXM = IXM
      N=N
      IF(IERROR-1) 57,57,560
      57   CALL INFNOS
      63   CALL IINOUT
            IBRS = IBRS
      IF(IERROR-1) 65,65,560
      65   CALL DEFLN
            I2=4*N+4
            CALL BEAM
            CALL DEFLN

```

```

K=N+1
KTEST = 0
MGE50073
MGE50074
MGE50075
MGE50076
MGE50077
MGE50078
MGE50079
MGE50080
MGE50081
MGE50082
MGE50083
MGE50084
MGE50085
MGE50086
MGE50087
MGE50088
MGE50089
MGE50090
MGE50091
MGE50092
MGE50093
MGE50094
MGE50095
MGE50096
MGE50097
MGE50098
MGE50099
MGE50100
MGE50101
MGE50102
MGE50103
MGE50104
MGE50105
MGE50106
MGE50107
MGE50108

210  DO 300 I1=1,IBRS
      IBSR=IBTAB(I1)
      DO 250 I3=1,IBRS
      IASR=IBTAB(I3)
      250  CONWT(IBSR) = (DEF(IASR)-XBRG(I3))*BNFLU(I1,I3)*(-1000.0)+*
      1 CONWT(IBSR)
      THETA(I1)=THETA(I1)-((DEF(IBSR)-XBRG(I1)))*BNFLU(25,I1)
      DEF(I1)=DEF(I1)-((DEF(IBSR)-XBRG(I1)))*BNFLU(24,I1)
      300  CALL DEFLN
      979  DO 400 I=1,IBRS
      J=IBTAB(I)
      IF(ABS(DEF(J)-XBRG(I))-0.001) 400,400,445
      400  CONTINUE
      IF(KTEST<-4) 410, 450, 450
      410  IF(ABS(BMTAB(I2))-100.)1420,2222,222
      420  IF(ABS(SFTAB(I2))-10.)1500,2222,222
      222  KTEST = KTEST +1
      CALL BEAM
      GO TO 979
      445  KTES2=KTES2+1
      IF (KTES2-4) 210, 450, 450
      450  WRITE (6,451) KTES2, KTEST
      451  FORMAT(27HOTNO MANY ITERATIONS - DEF1 14, 9H MOMENT 14)
      500  DO 515 I=1,K
      515  DIST(I)= 0.0
      IF (STIFX(I))515,515,514
      514  DIST(I)=1.E12/STIFX(I)
      515  CONTINUE
      800  DO 825 I=1,IBRS
      J=IBTAB(I)
      820  CONOT(I)=CONWT(I)
      825  CANOT(J)=CONOT(I)
      540  WRITE (6,1036) T1IL5,T1IL2

```

```
      WRITE (6,1040)
      DO 545 I=1,K
         IB = I+1
         IA = IB+IB
      545  WRITE (6,1050)
           NO(1),SFTAB(IA),BMTAB(IA),THETA(IB-1),DEF(1),CANOT(1)
           1      WRITE (6,1032)
           IXM = IXM
           IF(IXM)1222,1222,980
           GO TO(1222,1222,1222,1222,1222,1222,1221),IXM
  980      981      CALL GRAPH
           560      IF(IXM-7)1222,1222,1221
           1222      WRITE (6,1036)
           STOP
      END

```

```

S1BFTC REDS DECK
C READIN MGE5
C SUBROUTINE READIN
C SECOND CASE BEARING RAISED
C KEY FOR IXM SENTINEL
C BLANK .0 SINGLE CASE. LAST CASE - NO PLOT
C IXM - 1 NEW DENSITY
C C 2 NEW MODULUS
C 3 NEW DENSITY AND MODULUS
C 4 MULTIPLE WT RUN - SPEC CASE
C 5.6 SAME AS .0
C 7 PLOT SINGLE CASE
C 8 PLOT THEN MULTIPLE CASES
C 9 MULTIPLE CASES - ANOTHER FOLLOWS - NO PLOT
C VARIABLE NAMES USED IN READIN DO NOT MATCH REST OF PROGRAM
C DIMENSION A(401), B(401), C(401), D(401), E(401), F(401), G(401),
C 1K(401), L(401), IS(401), H(7), P(7), DIST(401), BMTAB(1620),
C 2THETA(802), DEF(401), BNFLU(25,25), DIBRG(25), IBTAB(25), SFTAB(1620),
C 3TITLE(12), TITLE(12), XBRG(25), NO(400),
C COMMON N, NO, A, B, C, D, E, I, J, K, L, IS, H, P, DIST, BMTAB, THETA, DEF,
C IBNFLU, DIBRG, IBTAB,
C 2 IBRS, SFTAB, I2, IERROR, TITL2, IXM
C DIMENSION NS(50)
C COMMON SWAT, NS, IYM
C COMMON TITL5, XBRG
C 10 FORMAT(13.5F12.4, 2I2, 3I1)
C 15 FORMAT(2I2, 2F12.2)
C 90 FORMAT(25H0 STATION DISTANCE ERROR 15)
C 91 FORMAT(24I3)
C P(6)=-0.0636
C P(7)=-0.03705
C DO 40 N=1, 400
C 22 READ(5, 10) NO(N), A(N), B(N), C(N), D(N), E(N), I(N), J(N), K(N), L(N), IS(N)
C IF(NO(N)-900)40, 40, 45
C 40 CONTINUE
C 45 NO(N) = NO(N) - 900

```

```

55 PI=3.14159265          RED50038
      N = N-1          RED50039
24      READ (5,15) IXM,IYM,AVIT,DAVIT          RED50040
      IF(IXM) 36,36,27          RED50041
      GO TO (29,28,81,36,36,36),1XM          RED50042
27      H(IYM)=DAVIT          RED50043
28      P(IYM)=AVIT          RED50044
29      GO TO 24          RED50045
      H(IYM)=AVIT          RED50046
      GO TO 24          RED50047
      SWAT=AVIT          RED50048
C      READ (5,91) (NS(II), II=1,IYM)          OPTION NOT ALLOWED IN CURRENT
36      DO 79 I3=1,N          RED50049
      DISTT(I3)=(A(I3+1)-A(I3))*.25          RED50050
      IF(DISTT(I3);82,56,56          RED50051
      82      WRITE (6,90) NO(I3)          RED50052
      TERROR = 2          RED50053
      GO TO 80          RED50054
56      AREA1=PI*(B(I3)**2-C(I3)**2)/4.0          RED50055
63      AM11=PI*(B(I3)**4-C(I3)**4)/64.0          RED50056
      IMAT=I(I3)          RED50057
      WT1=AREA1*P(IMAT)          RED50058
      STIF1=H(IMAT)*AM11          RED50059
      ST=STIF1          RED50060
      WAIT=WT1          RED50061
      IF(J(I3))65,66,65          RED50062
65      AREA2=PI*(C(I3)**2-D(I3)**2)/4.0          RED50063
      AM12=PI*(C(I3)**4-D(I3)**4)/64.0          RED50064
      JMAT=J(I3)          RED50065
      WT2=AREA2*P(JMAT)          RED50066
      STIF2=H(JMAT)*AM12          RED50067
      ST=STIF1+STIF2          RED50068
      WAIT=WT1+WT2          RED50069
66      IF(L(I3))70,75,70          RED50070
70      AREA3=PI*(B(I3)**2)/4.0          RED50071
      WT3=AREA3*P(7)          RED50072
                                      RED50073

```

WAIT=WAIT-WT3  
75 IF(I5(I3))77,78,77  
77 IF(D(I3))68,69,68  
69 WT4=(PI\*C(I3)\*\*2/4.0)\*P(6)  
GO TO 85  
68 WT4=(PI\*D(I3)\*\*2/4.0)\*P(6)  
85 WAIT=WAIT+WT4  
78 D(I3)=WAIT  
C(I3)=ST  
79 CONTINUE  
80 RETURN  
END

RED50074  
RED50075  
RED50076  
RED50077  
RED50078  
RED50079  
RED50080  
RED50081  
RED50082  
RED50083  
RED50084  
RED50085

MGE5 - SAMPLE INPUT FORM

COLUMN	1	1	2	2	3	4	4	5	6666667	7
123 5	3	6	4	8	5	0	6	2	4567890	3
RAISING BRGS 3•4•5•6 TO EQUALIZE OPERATING L.S. GEAR BRG. LOADS										
•020	•020	•0787	•1018	•0726						
9•0293	SAMPLE	CASE	12	BEARING SHAFT	4/1/64					
01	0•0	8•0								
02	2•0	8•0								
03	4•0	18•0								
04	12•5	18•0								
05	24•0	36•0								
06	40•5	36•0								
07	57•25	18•0								
08	68•5	18•0								
09	93•5	33•0								
10	98•5	18•0								
11	109•5	17•5								
12	122•75	31•0								
13	130•25	17•0								
14	306•5	17•0								
15	540•5	17•0								
16	590•75	31•0								
17	598•25	17•0								
18	774•5	17•0								
19	1008•5	17•0								
20	1058•75	31•0								
21	1066•25	17•0								
22	1242•5	17•0								
23	1476•5	17•0								
24	1526•75	31•0								

B. 8

25	1534.25	17.0	TMGE	
26	1698.50	17.0	TMGE	
27	1914.5	17.0	TMGE	
28	1968.5	34.0	TMGE	
29	2028.5	19.5625	TMGE	
30	2082.5	21.8125	19.5625	TMGE
31	2121.5	21.8125	19.5625	TMGE
32	2160.5	21.375	19.5625	TMGE
33	2371.0	21.8125	19.5625	TMGE
34	2443.0	21.8125	19.5625	TMGE
35	2515.0	19.5625	TMGE	
36	2543.5	19.5625	TMGE	
37	2559.5	16.0	TMGE	
938	2571.5		TMGE	
3 3	-0.28355	30000000.	TMGE	
07			TMGE	

Note: Material 3 as used is identical to Material 1 to illustrate the insertion of new material cards.

## MGE5 - SAMPLE OUTPUT SHEET

\*\*\* SHAFTING SYSTEM PROGRAM MGE5 \*\*\*

RAISING BRGS 3, 4, 5, 6 TO EQUALIZE OPERATING L.S. GEAR BRG. LOADS

SAMPLE CASE 12 BEARING SHAFT

4/1/64

STATION NO.	SHEAR FORCE (KIP.)	MOMENT (KIP-INCH)	SLOPE (RADIAN)	DEFLECTION (INCH)	REACTION (LBS.)
1	-0.	0.	-0.0000114	0.0201429	0.
2	-0.02851	-0.029	-0.0000114	0.0201201	0.
3	-0.05701	-0.114	-0.0000114	0.0200973	0.
4	19.95398	-3.205	-0.0000116	0.0200600	20624.3
5	19.12420	221.914	-0.0000038	0.0198969	0.
6	-8.73801	497.755	-0.000009	0.0198618	0.
7	-13.57237	310.906	0.000019	0.0198735	0.
8	6.79524	153.651	0.0000189	0.0200600	21170.4
9	4.99137	300.983	0.0000562	0.0200693	0.
10	3.77877	322.909	0.0000571	0.0211727	0.
11	2.98597	360.110	0.0000818	0.0219327	0.
12	2.08139	393.675	0.0001177	0.0233491	0.
13	0.47629	403.266	0.0001199	0.0261404	0.
14	7.88510	-512.433	0.0002805	0.02788999	10782.3
15	8.83585	-429.372	-0.000567	0.0181795	16011.0
16	5.60175	-66.026	-0.0001526	0.01959228	0.
17	3.99664	-36.034	-0.0001528	0.01947786	0.
18	7.73229	-325.870	-0.0001694	0.0275983	15000.0
19	8.71686	-278.822	-0.0001858	0.0264957	16000.0
20	5.48276	78.243	-0.0002210	0.0184674	0.
21	3.87765	113.345	-0.0002205	0.0168116	0.
22	6.98398	-202.864	-0.0000459	0.0098087	14600.0
23	8.46648	-330.665	0.0000653	0.0080157	16000.0
24	5.23238	13.519	-0.0000539	0.00918265	0.
25	3.62277	46.742	-0.0000538	0.0092308	0.
26	6.29193	-225.635	0.0000200	0.0080253	13000.0
27	15.74768	-367.973	-0.0000618	0.0090382	23000.0
28	12.27223	388.564	-0.0000504	0.0045619	0.
29	-3.17422	661.504	-0.0000320	0.0070765	0.
30	-7.17504	382.074	0.0001031	0.0048424	0.
31	5.02966	30.504	0.0001341	0.0080538	15000.0
32	1.35050	154.917	0.0001490	0.0064096	0.
33	-17.64255	-1559.821	-0.0001482	0.0297004	0.
34	35.02733	-3074.609	-0.0001745	0.0060024	59461.9
35	28.23410	-797.196	-0.0012424	0.0752218	0.
36	1.78015	-22.587	-0.0012959	-0.1116345	0.
37	0.59473	-3.598	-0.0012957	-0.1323769	0.
38	-0.03002	-0.019	-0.0012959	-0.1479388	0.

\* WITH CERTAIN BEARINGS LOWERED OR RAISED FROM ORIGINAL STRAIGHT LINE DATES

## APPENDIX C

### NOTES ON MODIFICATION FOR OTHER COMPUTER SYSTEMS

1. A programmed double-precision arithmetic was used internally in matrix inversion on 7090. A computer with greater significance might use a single-precision version, or the LARC version **MAT2L** might be modified to avoid the assembly language subroutine.
2. Use of SC 4020 option assumes a library of **MAP** coded routines available on NSRDC system tape. A **FAP** version of these routines exists.
3. For **FORTRAN II** use insert **F** on library and open subroutine names as follows:

**MGE2 0104, 0108, 0109**  
**MAT2 0040, 0037**

A **FAP** version of **DPAF** also exists. Card **MGE2 0159** may be changed to reflect standard system stop; e.g., **CALL EXIT**.
4. Total allowed number of stations (400) would handle an aircraft carrier. For a smaller computer, all dimensions of **400, 401 802, and 1620** may be reduced equivalently.

Card **RED2 0032**  
or           **RED5 0032**

must reflect the maximum allowed number of stations.

## REFERENCES

1. Antkowiak, Edward T., "Calculation of Ship Propulsion Shafting Bearing Reactions on an IBM 650 Computer," Boston Naval Shipyard Report R-11 (1967).
2. Anderson, H. C., et. al., "Shafting Systems Programs MGE-402 and MGE-405, "DR59MSD-202, General Electric Company, Lynn, Massachusetts (1959).
3. Luvisi, Joseph, "Calculation of Ship Propulsion Shafting Bearing Reactions on a Datatron 205 Computer," Boston Naval Shipyard Report R-24.

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